Drainage Report - Final

Adeles Acres Subdivision

March 2, 2023 (Revised -----)

Prepared by:



215 Pitkin Ave, Unit 201 Grand Junction, CO 81501 Phone: (970) 241-4722 Fax: (970) 241-8841

Job No. 2060-001

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Engineer's Certification

I hereby certify that the Drainage Report for the design of **Adeles Acres Subdivision** was prepared by me, or under my direct supervision, in accordance with the provisions of the Grand Junction Municipal Code Title 28 STORMWATER MANAGEMENT MANUAL (SWMM), for the owners thereof. I understand that the **City of Fruita** does not and will not assume liability for drainage facilities designed by others.

Jeff Mace, P.E. State of Colorado Reg. No. 37343

Developer's Certification

I, hereby conformation the Adeles Acres Subdivision shall be constructed in this report. I understand that the City of but cannot, on behalf of the Adeles Acres Subdivision drainage design review will absolve Futurado Desuccessors and/or assigns of future liability for improper	Fruita reviews drainage plans guarantee that the preliminary velopment LLC and/or their
(THIS PAGE WILL BE SIGNED FOR FINAL SUBMITTAL	.) (Name of Developer)
	(Authorized Signature)
	(Date)

I. Introduction

A. Background

The purpose of this Drainage Report is to identify pre-development and post-development drainage conditions for the proposed Adeles Acres Subdivision. This report identifies the following items with respect to the site:

- · existing drainage patterns and issues
- developed drainage patterns
- potential drainage issues resulting from development
- solutions to the potential drainage issues
- design of the various elements of the storm drain system for the site
- water quality requirements for developed runoff
- post construction BMP's

This report is intended to show the full-buildout feasibility of the proposed Adeles Acres Subdivision development project. Any phasing of construction progress shall follow the overall proposed drainage patterns outlined in this report, while providing temporary means to convey runoff to the desired outfall(s), using temporary BMP's as needed.

B. Project Location

The proposed project site is located at the southeast corner of the intersection of 19 Road and J.2 Road in Fruita, Colorado. The current project address is **1024 19 Road**, **Fruita**, **CO 81521 (Parcel No. 2697-153-00-181)**. In more legal terms, the project site is in the north half of the SW ¼ of the SW ¼ of Section 15, Township 1 North, Range 2 West of the Ute Meridian, Mesa County, Colorado. Refer to **Figure 1** for the General Location Map of the proposed development.

Access to the project site will be from the south side of J.2 Road at the proposed entrance for the development (proposed Lily Street). Currently, J.2 Road is a two-way gravel road east of 19 Road, and a two-lane paved road west of 19 Road. 19 Road is a two-way paved road with gravel shoulders. The proposed project parcel is occupied by a single residence and shows signs of recent livestock activities. Onsite structures include fencing, small sheds, a garage, a house, and a tall cell phone tower near the northwest corner of the property.

The surrounding area contains a mix of uses, including single family residential and agricultural uses. The proposed project site is zoned Agricultural, along with the parcels located directly to the north, west, south, and northwest. The Palmer Subdivision is located directly to the east and southeast and is zoned Residential.

C. Project Description

The project parcel is approximately 15.01 acres of agricultural use consisting of livestock activities and crop cultivation with a single-family residence present. This parcel is being subdivided into 48 single-family residential lots, with supporting right-of-way (ROW), Homeowner's Association Tracts, and easements for utility and access agreements. The project parcel is bounded on the west by 19 Road, on the North by

J.2 Road, on the east and southeast by the Palmer Subdivision, and on the south by Parcel No. 2697-153-01-001.

Existing vegetation at the proposed project site consists of desert shrubs and brushes in fair condition (~50% cover), along with several cottonwoods and other deciduous trees dispersed across the property. The existing residence has landscaping and a grass lawn around the house. The property is approximately split into thirds by existing wood and wire fencing. The eastern third of the property appears to be undeveloped rangeland with natural desert vegetation. The western third has a large cell phone tower, a residence, several sheds, and mostly bare ground. The middle-third of the property shows signs of livestock activities and/or horse boarding. Web Soil Survey obtained from the NRCS web site shows soils present at the site consist entirely of Fruitland sandy clay loam (0-2% slopes). Fruitland sandy clay loam is classified as Hydrologic Soil Group B. Group B soils have slower infiltration rates than Group A soils, and higher infiltration rates than Group C and Group D soils. NRCS Soil information is included in Appendix A.

The proposed development is entirely within the 117 Major Drainage Basin in Mesa County, CO. The 117 Major Drainage Basin flows to the Colorado River, approximately 1.5 miles south of the site. A graphical representation of the project boundary in relation to the major drainage basins is provided with **Figure 2**. There are no mapped FEMA Floodplains within or adjacent to the project site. A FEMA FIRM Map for the area is available in Appendix A.

D. Previous Investigations

No previous investigations involving the project parcel are known to exist.

II. Drainage System Description

A. Existing Drainage Conditions

Existing topography at the site consistently slopes from northeast to southwest with typical grades ranging between 0.5% and 2.0%. Earthen berms and private irrigation ditches border the project parcel on the north, east, and parts of the southern boundary. These existing features act as drainage boundaries keeping offsite runoff from entering the proposed project parcel and maintaining historic drainage patterns.

A roadside swale on the east side of the 19 Road corridor carries local runoff to the south along the western boundary of the project parcel. Runoff generated from the project area travels from east-to-west and ultimately discharges at the southwest corner of the parcel into the roadside swale. The swale drains south within the 19 Road corridor to an existing irrigation structure at the northeast corner of the J Road & 19 Road intersection. From there, flows are conveyed west and collected into the Grand Valley Drainage District's (GVDD) Coup Drain. All runoff generated from the proposed development is within the 117 Major Drainage Basin in Mesa County, and ultimately tributary to the Colorado River approximately 1.5 miles south of the project site.

For analysis of the existing site conditions, the project area has been evaluated with existing topography and imagery available from the Mesa County GIS website, as well as topographic survey information collected specific to this project. The project area

has been divided into separate sub-basins representing the various flow paths and tributary areas for each identified drainage design point. Two separate sub-basins have been delineated for the existing conditions analysis of the proposed development project. Refer to **Figure 3** for a layout of the existing conditions sub-basins and design points in relation to the project parcel. **Table 1** provides a summary of the existing conditions sub-basins that were delineated and analyzed for this project.

Table 1: Existing Conditions Sub-Basin Information

Sub- Basin	Design Point	Area (acres)	Soil Group	Percent Impervious	Design Storm Peak Runoff Rates (f Rates (cfs)
ID	Tonic	(uorco)	Gloup	inipervious	2-Year	10-Year	100-Year
EC-01	E1	14.55	В	5%	0.22	0.94	2.82
EC-02	E2	0.72	В	24%	0.02	0.44	0.89

B. Master Drainage Plan

No "Master Drainage Plan" is known to exist for the subject property.

C. Offsite Tributary Area

Runoff from the south side of the J.2 Road corridor flows into a small existing roadside drainage swale located between the edge of gravel road and the north edge of the concrete irrigation ditch. The swale carries corridor runoff west to the intersection with 19 Road where flows in excess of the roadside swale capacity are captured by the adjacent irrigation ditch and carried west through the culvert crossing underneath 19 Road. Analysis of local runoff contributing to this historic project discharge point is provided in the existing conditions and proposed conditions analysis of this project. Additional flows carried by the existing irrigation ditch have not been quantified as part of this project, as those are considered undeveloped pass-through flows for the project site.

D. Proposed Drainage System Description

The proposed project will include lot grading, vertical curb and gutter, back lot drainage, storm drain, and a detention pond with outlet structure. Runoff from the developed areas will sheet flow to the curb and gutter sections of the proposed road or to the back-lot v-pans. From there, runoff will be directed to storm drain inlets where it will be collected and conveyed through the site to the stormwater pond at the western end of the development. The proposed grading and layout of the subdivision divides the project site into several separate sub-basins used for the developed conditions analysis of the project.

Seven separate sub-basins have been delineated and analyzed for the proposed conditions analysis of the proposed development. Refer to **Figure 4** for a layout of the proposed sub-basins in relation to the project parcel. Design runoff calculations for each of the sub-basins associated with the project have been completed using the Rational method as outlined in section 28.28 in the SWMM. Detailed information about sub-basin breakdown, site imperviousness, and Rational runoff coefficient calculations are provided in Appendix B. **Table 2** provides a summary of the proposed sub-basins that were delineated and analyzed as part of this project.

Table 2: Proposed Conditions Sub-Basin Information

Sub-Basin ID	Design Point	Area (acres)	Soil	Percent	Design Storm Peak Runoff Rates (cfs)		
ID.	Tollic	(acres)	Group	Impervious 2-Year		10-Year	100-Year
DC-01	D1	7.35	В	61%	3.47	6.65	14.66
DC-02	D2	2.05	В	64%	1.16	2.20	4.64
DC-03	D3	1.56	В	55%	0.81	1.62	3.76
DC-04	D4	0.98	В	10%	0.06	0.25	1.54
DC-05	D5	2.62	В	20%	0.26	0.72	2.91
DC-06	D6	0.75	В	19%	0.09	0.26	0.75

The proposed detention pond is a permanent stormwater solution designed to adequately provide water quality and stormwater detention measures for the Adeles Acres Subdivision. The pond is positioned within HOA Tract A of the development. The pond has been designed to hold the required water quality capture volume (WQCV), while providing detention storage for excess runoff during the 10-year and 100-year storm events. **Table 3** provides a summary of calculated water surface elevations and associated stage-storage volumes within the proposed detention pond for each design event.

Table 3: Pond Water Surface Elevation and Volume Summary

Event	Elevation	Volume (ft³)
Top of Pond	4,545.20	52,287
100-Year WSEL	4,542.66	19,618
Top of Structure	4,542.21	16,881
10-Year WSEL	4,541.42	8,890
Pond/Structure Bottom	4,539.16	0

A Geotechnical Report for the project area was performed by Huddleston-Berry in January 2023. The report includes analysis of two test pit sites in the area of the proposed detention pond. Excerpts from the Geotechnical Report are included in the Appendix. The report shows groundwater to be present at approximately 8 feet below the existing ground surface in the location of the proposed detention pond. The proposed pond bottom has been kept approximately 1.5 feet higher than the discovered groundwater table to prevent seepage.

The project parcel has two separate project discharge points where concentrated stormwater runoff leaves the site. One discharge point is an irrigation ditch at the northwest corner of the parcel where the ditch is piped underneath 19 Road to the west. The second discharge point is near the southwest corner of the parcel where surface flows join the 19 Road roadside drainage swale flowpath on the east side of 19 Road. Should the pond outlet system become clogged or unfunctional, there is adequate freeboard in the proposed pond to hold the runoff from storm events ranging in intensities up to the 100-year storm event. Should the pond ever be overtopped,

proposed and existing grades will direct overflow southwest to the existing historical drainage point at the southwest corner of the parcel. **Table 4** provides the existing and proposed discharge rates for the development. Refer to Figures 3 and 4 for Project Discharge Point locations.

Table 4: Project Discharge Rates

Project	Project Discharge	Contributing	Contributing	Peak Flow at Discharge Point		
Discharge Point ID	Point Location Description	Design Points to Project Discharge Point	Sub-basins to Project Discharge Point	Minor Storm 10-Year (cfs)	Major Storm 100-Year (cfs)	
Z1	Existing Conditions - Southwest Property Boundary	E1	EC-01	1.19	9.09	
N2	Proposed Conditions - Southwest Property Boundary	D6 & D8	DC-01, DC-02, DC-03, DC-04, DC-05 & DC-06	2.12	9.05	
Z2	Existing Conditions - J 2/10 Road Drain Culvert	E2	EC-02	0.64	1.09	
N3	Proposed Conditions - J 2/10 Road Drain Culvert	D7	DC-07	0.64	1.10	

Per SWMM requirements, the proposed discharge rates for the project have been kept to historic flow rates (existing conditions flow rates). As shown in Table 4, developed conditions and existing conditions peak flows are approximately the same. Although project discharge point N3 shows an increase of 0.01 cfs during the 100-year runoff event, this amount of flow is considered negligible per standard engineering practices.

E. Drainage Facility Maintenance

Ownership and maintenance of the proposed drainage improvements within public ROW shall be by the City of Fruita. All storm drain, the detention pond, and other drainage facilities within Property Owner's Association tracts and easements and will be owned and maintained by the Property Owner's Association. Inspection of the drainage facility and associated BMP's shall be as per Sections 28.16.120 and 28.64.130 of the Stormwater Management Manual (SWMM).

The developed drainage for the site has been designed to minimize maintenance; there are no mechanical items to check and maintain (i.e., pumps). Anticipated maintenance includes periodic (1-2 times per year and as needed after major storm events) clearing of debris from drains, trash racks, and the water quality orifice plate. Periodic sediment removal from the pond and outlet system may be required. The removal frequency will vary depending on the sediment removal loading through the system to the detention pond, but it is unlikely sediment removal would be required more often than once every 5 to 10 years.

III. Drainage Analysis and Design Criteria

A. Regulations

The policy, design criteria, design constraints, methods of analysis, recommendations, and conclusions presented in this report are in conformance with standard engineering practice and the Stormwater Management Manual.

B. Development Criteria

No drainage constraints were noted for this project.

C. Hydrologic Criteria

The hydrologic design criteria presented in this report are in conformance with standard engineering practice and the Stormwater Management Manual, except as noted within the report.

D. Hydraulic Criteria

The hydraulic design criteria presented in this report are in conformance with standard engineering practice and the Stormwater Management Manual, except as noted within the report.

E. Variance from Criteria

No variances from the SWMM are requested for this project.

F. Calculation Methodology

Rational method calculations have been used to model basin runoff for this project. Autodesk Storm and Sanitary Analysis 2022 has been used to model the routing hydraulics. The Mile High Flood District Detention Basin Design Workbook has been used for the Pond modeling and outlet structure design. The Autodesk software and selected methods are all accepted by the regulatory and engineering community and are within standard engineering practice.

G. Calculation and Modeling Results

Analysis results of the proposed site drainage conditions are included in the Appendix and highlighted below.

1. Design Storms

Major and Minor Design Storm Runoff associated with this project has been calculated with the Rational method, as outlined in Section 28.28.100 of the SWMM. Site specific precipitation depth information used for analysis of this project has been downloaded from the NOAA Atlas 14 online server. NOAA Precipitation data is provided in Appendix A. Rational method runoff calculations are provided in Appendix B.

2. Sub-Basins

Two existing sub-basins have been analyzed for the existing conditions analysis of the project site. Seven separate sub-basins have been analyzed for the fully developed conditions analysis of the proposed subdivision. Sub-basin layouts for the existing and

developed conditions, along with design storm peak flows for each sub-basin, are shown on **Figures 3** and **4**, respectively.

3. Storm Drain Pipes

The proposed drainage system requires several storm drain pipes and structures. **Table 5** provides a summary of the proposed storm drain pipes needed for the full buildout of the proposed subdivision. As shown, velocities for all proposed pipes are within SWMM criteria.

Tah	le 5°	Propose	d Storm	Drain Pi	nes
ıav	IC J.	LIOPOSE	u otomii	Diamiri	DCO

Pipe ID	Pipe Material	Pipe Diameter	Pipe Length	Pipe Slope	2-yr Peak Flow in Pipe	2-yr Max Velocity in Pipe	100-yr Peak Flow in Pipe	100-yr Max Velocity in Pipe	Max Flow Depth/ Total Depth Ratio
		(inches)	(ft)	(%)	(cfs)	(ft/sec)	(cfs)	(ft/sec)	(ft)
K1-K2	RCP	24.0	60.0	0.50	4.31	3.86	18.13	5.77	1.00
K2-K3	RCP	24.0	119.0	0.50	4.33	3.58	18.13	5.77	1.00
K3-K4	RCP	24.0	31.0	0.50	3.46	2.82	14.60	4.65	1.00
L1-L2	RCP	18.0	115.0	0.50	0.78	2.63	3.67	3.92	0.98
M1-M2	RCP	18.0	101.0	0.40	0.08	1.21	2.28	3.52	0.46
N1-N2	RCP	18.0	85.3	0.40	0.08	1.25	2.29	3.14	0.43
N2-N3	RCP	18.0	685.0	0.40	0.08	1.28	2.33	3.30	0.43
N3-N4	RCP	18.0	645.0	0.40	0.08	1.36	2.32	3.66	0.41
N4-N5	RCP	18.0	475.0	0.30	0.08	1.19	2.31	3.37	0.44
N5-N6	RCP	18.0	451.0	0.30	0.08	1.15	2.31	3.47	0.45

4. Storm Drain Inlets

The proposed drainage system requires several storm drain inlets to collect stormwater runoff. **Table 6** provides a summary of the proposed storm drain inlets for the proposed development during the minor (2-year) and major (100-year) storm events, respectively.

Table 6: Proposed Storm Drain Inlets

Inlet ID	Туре	Sump, or On-Grade Min Slope (%)	Grate Elevation (ft)	Max HGL Elevation Attained (ft)	Invert Elevation (ft)	2-Year Peak Flow to Inlet (cfs)	100-Year Peak Flow to Inlet (cfs)
SDCI-K3	Double Inlet	Sump	4,544.12	4,544.09	4,540.67	1.16	4.64
SDCI-K4	Double Inlet	Sump	4,544.12	4,544.55	4,540.82	3.47	14.66
SDCI-L2	Single Inlet	Sump	4,544.35	4,542.69	4,541.25	0.81	3.76

As shown, the hydraulic grade line does not exceed the grate or the allowable ponding depth of any proposed inlets during the 100-year design storm event. All inlet capacities are adequate, per SWMM inlet capacity charts provided in the Appendix. As shown on the capacity charts, Double Curb Inlets have a capacity to capture 15.4

cfs while meeting 100-year design storm criteria, which includes a 1.0-foot ponding depth above the flowline or grate elevation of the inlet (SWMM section 28.44.130). At the low-point of the proposed subdivision road where SDCI-K3 & SDCI-K4 are positioned in the proposed storm system layout, the ponding of water will overtop the road crown before reaching a depth of 0.5 feet and spill into the double inlet on the other side (West side) of the road (SDCI-K3). Developed conditions flow analysis shows that SDCI-K3 would have enough capacity as a single curb inlet to handle the half-street flows directed to it. However, SDCI-K3 has been intentionally oversized to be a double curb inlet at the low-point to provide the extra capture capacity for accepting spill-over flows from the east side of the road. The combined capture capacity at the low point is expected to adequately keep flow/ponding depths within SWMM criteria.

5. Hydraulic Grade Line

The hydraulic grade line (HGL) does not exceed the grate elevations of the proposed inlets (or manholes) during all design storm events, per SWMM criteria. Detailed hydraulic modeling output for each design storm is provided in the Appendix. Profile views of each storm line during the 100-year design storm event are also provided in the Appendix.

6. Street Capacity

Street capacities for the street sections were checked based on the 100-year design storm peak flow rates generated for the maximum combined flow to a half-street section during fully developed conditions. There are no issues with half-street conveyance capacity for each sub-basin, per SWMM Figures 28.44.100(a). See the SWMM half-street capacity sheet provided in the Appendix for more detail.

7. Outlet Protection

Maximum peak discharge rates have been analyzed for all storm outfalls to determine the need for riprap protection. Detailed riprap calculations are provided in the Appendix for the fully developed conditions of the subdivision. Riprap locations and dimensions are shown on the construction plans.

IV. Post Construction Stormwater Management

A. Stormwater Quality Control Measures

The detention pond for this project has been designed to hold the 100-year storm event, including the WQCV, without overtopping. The Mile High Flood District Detention Basin Design Workbook was used to help design the pond outlet structure configuration for this project. The pond acts as an extended detention basin that treats the WQCV and drains the pond within SWMM guidelines. Discharge rates from the pond are metered by the outlet works to not exceed historic conditions. Detention Basin Design Workbook calculations and Pond Drain Times are provided in Appendix B of this report.

B. Stormwater Quality Calculations

The WQCV was determined based on the percent imperviousness of the fully developed subdivision and all areas tributary to the proposed detention pond. WQCV was calculated using Section 28.64.100 in the SWMM. WQCV calculations are provided in Appendix B of this report.

V. Conclusions

A. Compliance with Manual

The policy, design criteria, design constraints, methods of analysis, recommendations, and conclusions presented in this report are in conformance with standard engineering practice and the Stormwater Management Manual.

B. Design Effectiveness

This design will be very effective for controlling runoff from this site and will provide stormwater quality measures.

C. Areas in Flood Hazard Zone

There are no areas within the proposed project site that are classified as Flood Hazard Zones. There are no floodplains within the project area.

D. Variances from Manual

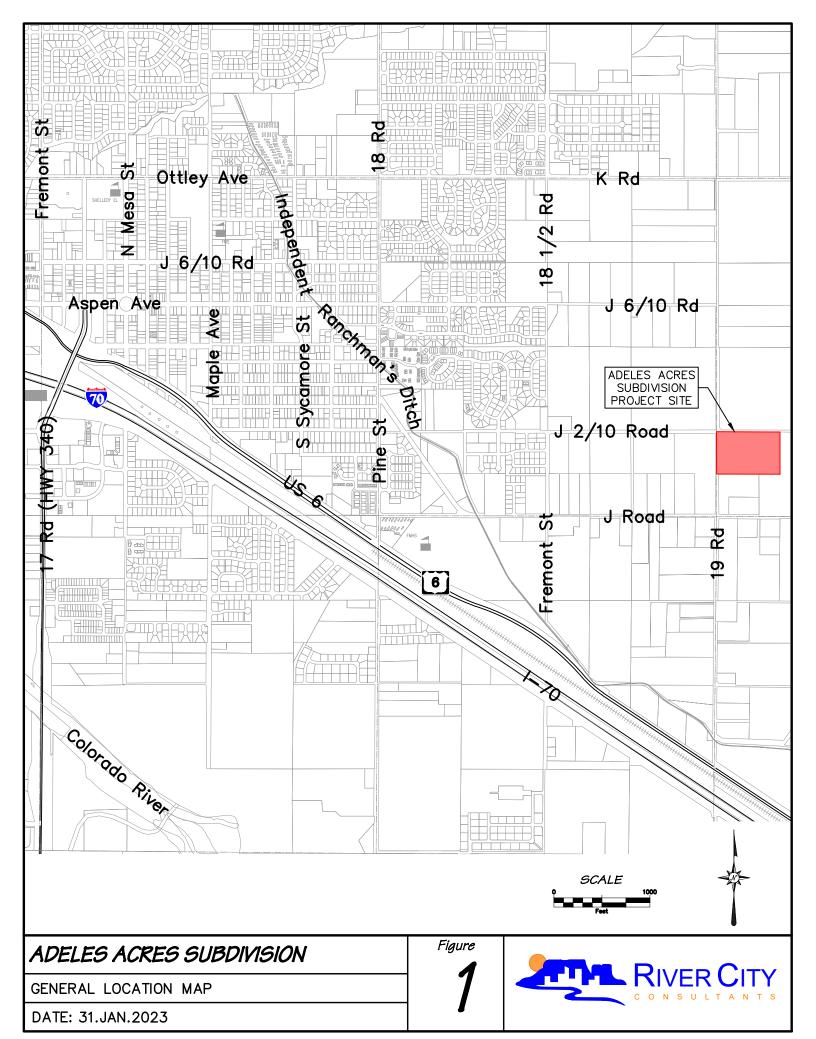
No variances from the manual are requested for this project.

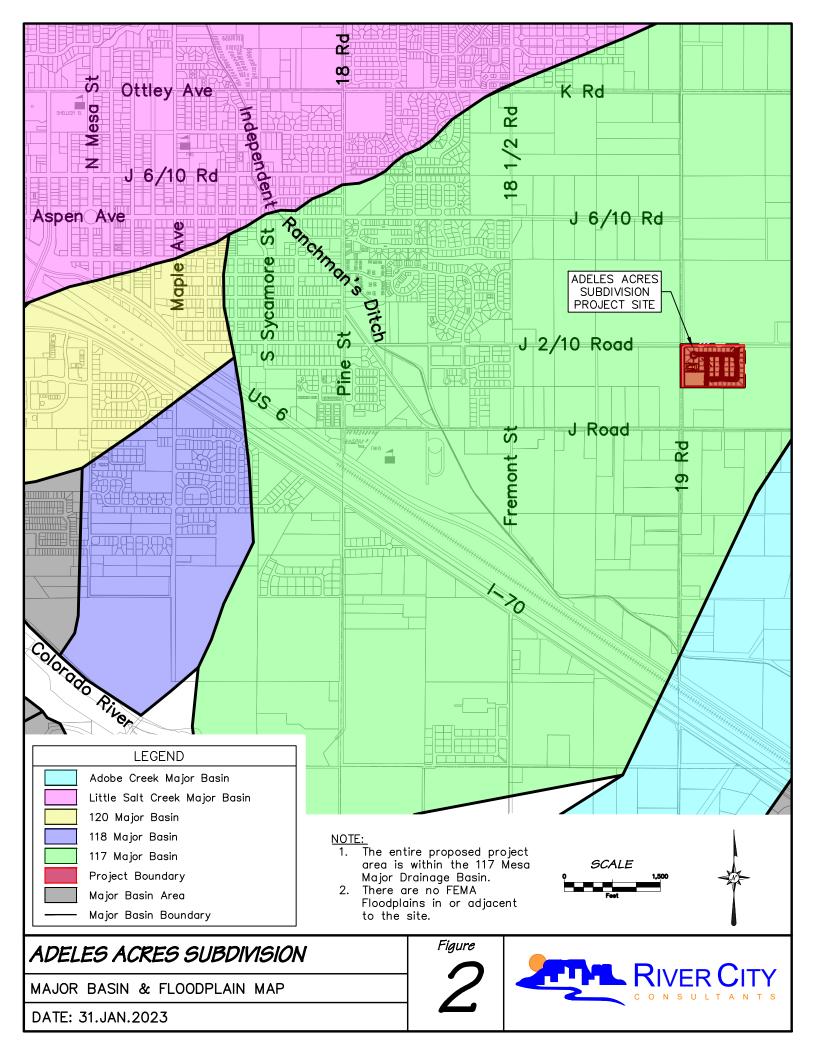
VI. References

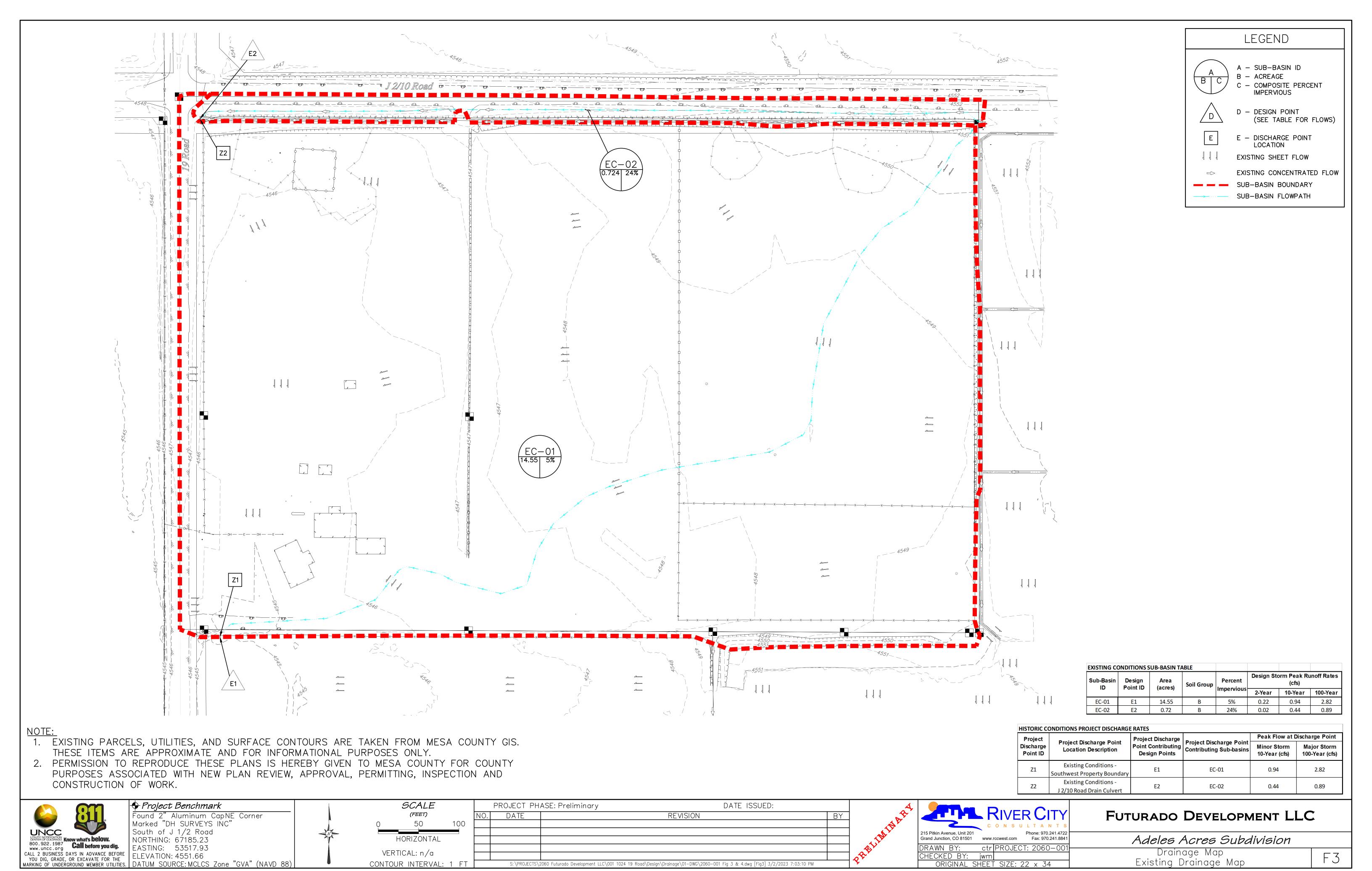
- 1. Grand Junction Municipal Code Title 28 STORMWATER MANAGEMENT MANUAL (SWMM), Title 28 STORMWATER MANAGEMENT MANUAL (codepublishing.com)
- 2. City of Fruita GIS Website, City Map (fruita-gis.maps.arcgis.com)
- 3. Mesa County Colorado GIS Website, https://gis.mesacounty.us/.
- 4. Natural Resources Conservation Service National Cooperative Soils Survey Website, http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx .
- 5. FEMA Flood Map Service Center website, https://msc.fema.gov/portal.
- Geotechnical and Geologic Hazards Investigation 1024 19 Road, Fruita, Colorado, Project #02594-0001, January 12, 2023, Huddleston-Berry Engineering & Testing, LLC.
- 7. Urban Storm Drainage Criteria Manual, Volumes 1, 2, & 3; Mile High Flood District, Denver, Colorado; originally published 1969 and revised January 2021.
- 8. Mile High Flood District Detention Basin Design Workbook, Version 4.05 (January 2022).

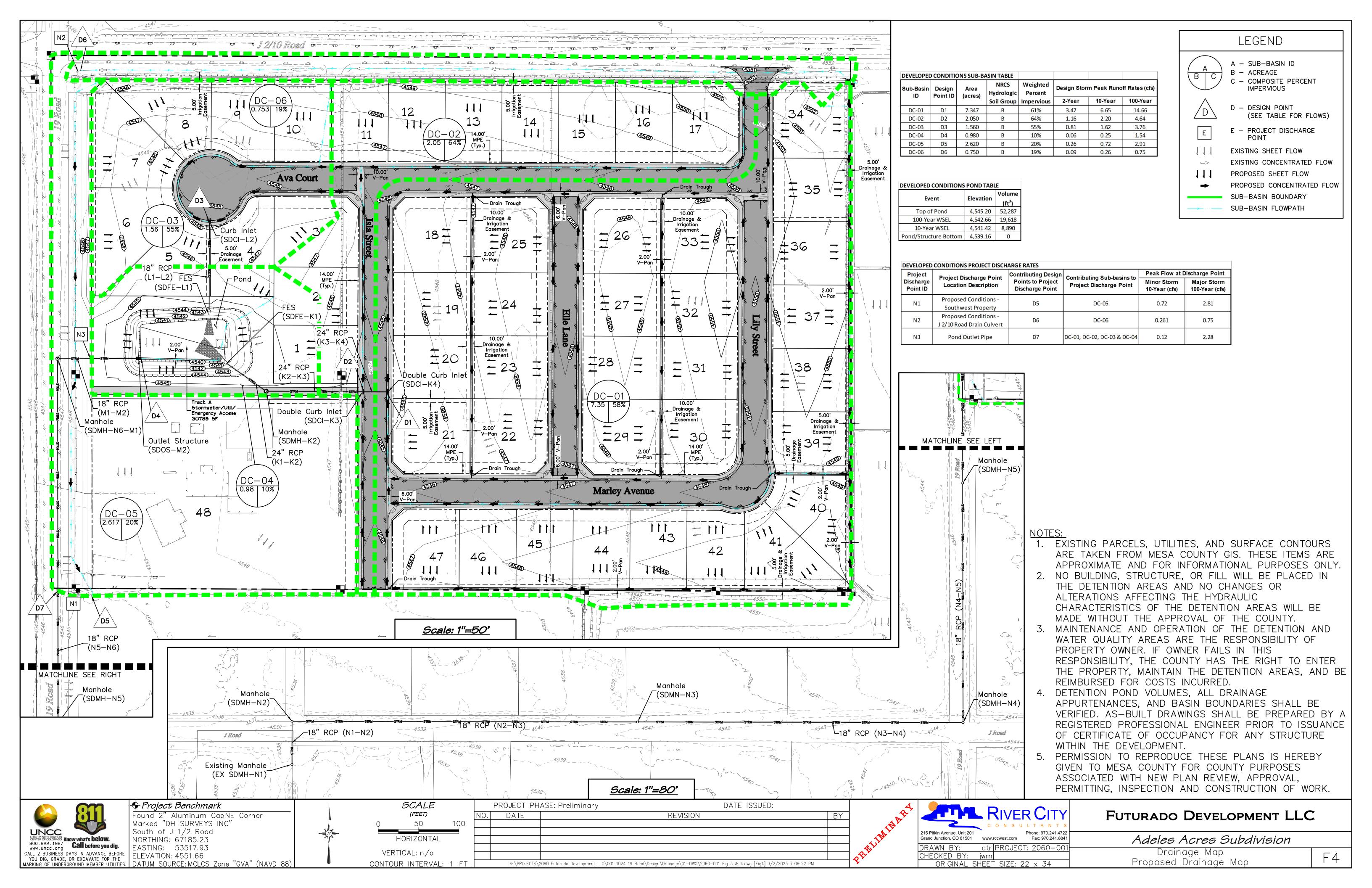
FIGURES

- 1. General Location Map
- 2. Major Basin & Floodplain Map
- 3. Existing Conditions Drainage Map
- 4. Developed Conditions Drainage Plan









APPENDIX A

Project Site Information

- 1. FEMA FIRM Panel
- 2. NRCS Web Soil Survey
- 3. NRCS K Factor Whole Soil
- 4. NOAA Atlas 14 Precipitation Depths
- 5. Geotechnical Report Excerpts

NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for ossible updated or additional flood hazard information.

obtain more detailed information in areas where **Base Flood Elevations** (BFEs Nor **floodways** have been determined, users are encouraged to consult the Floo and/or floodways have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) Report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot levations. These BFEs are inhered for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, road elevation data presented in the FIS Report should be utilized in conjunction with ne FIRM for purposes of construction and/or floodplain management.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study Report for information on flood control structures for this jurisdiction.

Coastal Base Flood Elevations shown on this map apply landward of 0.0' Vorth American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be ware that coastal flood elevations are also provided in the Summary of Stillwater levations table in the Flood Insurance Study Report for this jurisdiction. Elevations hown in the Summary of Stillwater Elevations table should be used for construction nd/or floodplain management purposes when they are higher than the elevations hown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study Report

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD 83, GRS80 spheroid Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same verifical datum. For information regarding convention between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at https://www.ngs.ngaa.gov or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282 '301) 713-3242

o obtain current elevation, description, and/or location information for **bench mark** hown on this map, please contact the Information Services Branch of the Nations Seodetic Survey at (301) 713-3242, or visit its website at http://www.ngs.noaa.gov.

Base map information shown on this FIRM was derived from NAIP color infrared orthophotography produced with a one meter ground resolution from shotography dated 2003 or later.

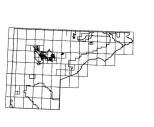
Based on updated topographic information, this map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous PIRM for this jurisduction. As a result, the Ploud Profiles and Floodway Data tables for multiple streams in the Flood insurance Study Report (which contains authoritative hydratilic data) may reflect stream channel distances that differ from what is shown on the map. Also, the road to floodplain relationships for unrevised streams may differ from what is wn on previous maps.

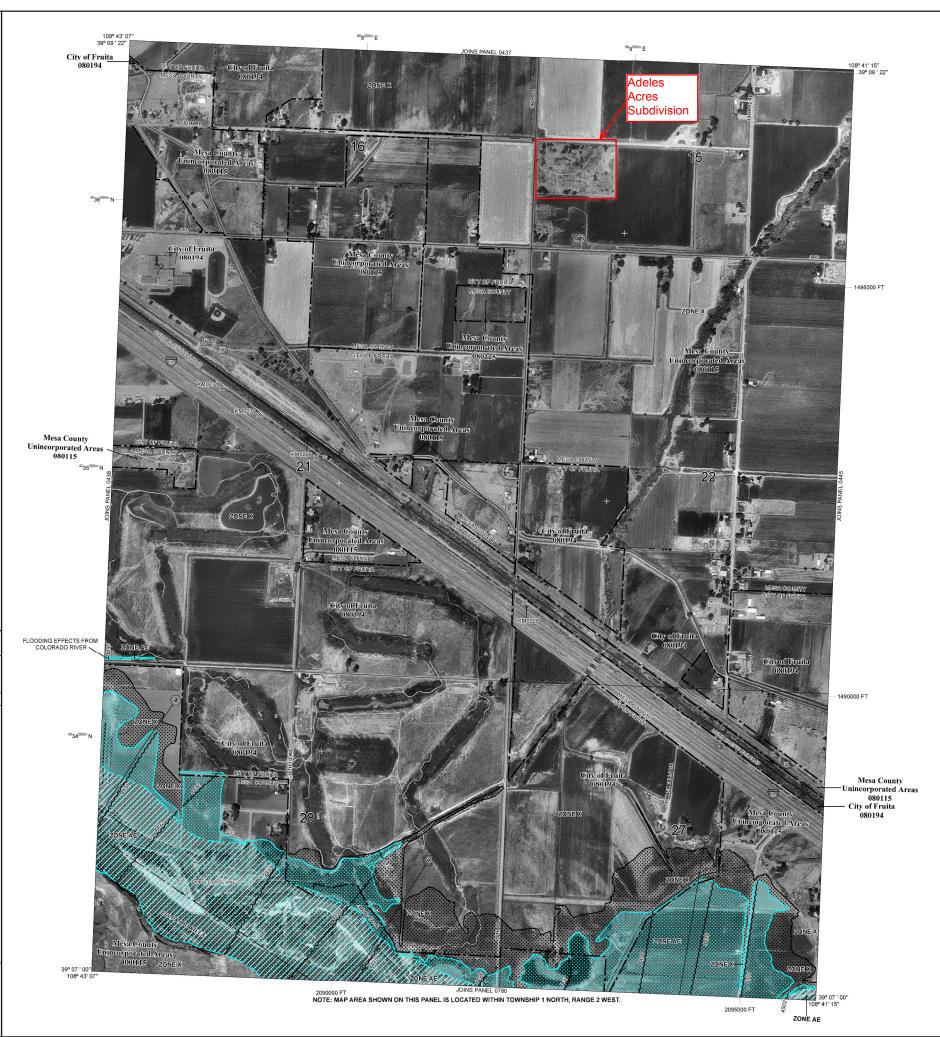
Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and digital versions of this map. The FEMA Map Service Center may also be reached by "ax at 1-800-359-8520 and its website at http://www.msc.fema.gov/

If you have **questions about this map** or questions concerning the National Floor Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at http://www.fema.gov.

Mesa County Vertical Datum Offset Table								
Flooding Source	Vertical Datum Offset (ft)	Flooding Source	Vertical Datum Offset (ft)					
Colorado River	3.4							





LEGEND

SPECIAL FLOOD HAZARD AREAS (SHIAs) SUBJECT TO INUNDATION BY THE 19% ANNUAL CHANCE FLOOD

The 19% annual charact floot (100)-war flood, also known as the base flood, is the flood that has a 19% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to tolonging by the '9% annual character flood. Areas of special Flood hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 19% annual character floor.

ZONE A No Base Flood Elevations determined. ZONE AE Base Flood Elevations determined.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. ZONE AH

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determine ZONE AR

Special Pixod Hearth Areas formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

ZONE A99 Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.

Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations

ZONE VE

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood helpits.

OTHER FLOOD AREAS

ZONE X

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS ZONE X

Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS), AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas

1% annual chance floodplain boundary 0.2% annual chance floodplain boundary Floodway boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

Base Flood Elevation line and value: elevation in feet* (EL 987)

Base Flood Elevation value where uniform within zone; elevation in

*Referenced to the North American Vertical Datum of 1988 $\langle A \rangle$ —⟨A⟩ Cross section line

23 - - - - - - - - 23 45° 02' 08", 93° 02' 12"

1000-meter Universal Transverse Mercator grid values, zone 12 5000-foot ticks: Colorado State Plane coordinate system, Central zone (FIPSZONE 0502), Lambert Conformal Conic projection Bench mark (see explanation in Notes to Users section of this FIRM panel)

DX5510 × *M1.5

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP July 6, 2010

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL



MAP SCALE 1" = 500' 250 0 500 1000 FEET 150 0

PANEL 0439F FIRM FLOOD INSURANCE RATE MAP MESA COUNTY, COLORADO AND INCORPORATED AREAS PANEL 439 OF 1725 (SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS: COMMUNITY FRUITA, CITY OF MESA COUNTY NUMBER PANEL SUFFIX 080194 0439 F 080115 0439 F Notice to User: The **Map Number** shown below should be used when placing map orders; the **Community Number** shown above should be used on insurance applications for the subject MAP NUMBER 08077C0439F EFFECTIVE DATE JULY 6, 2010 Federal Emergency Management Agency

National Flood Hazard Layer FIRMette

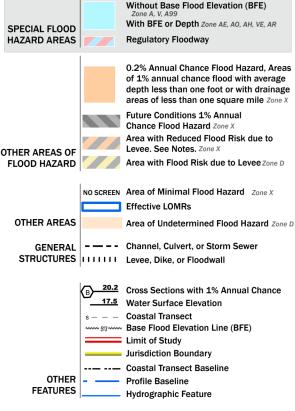


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



MAP PANELS

No Digital Data Available

Unmapped

The pin displayed on the map is an approximate

an authoritative property location. This map complies with FEMA's standards for the use of

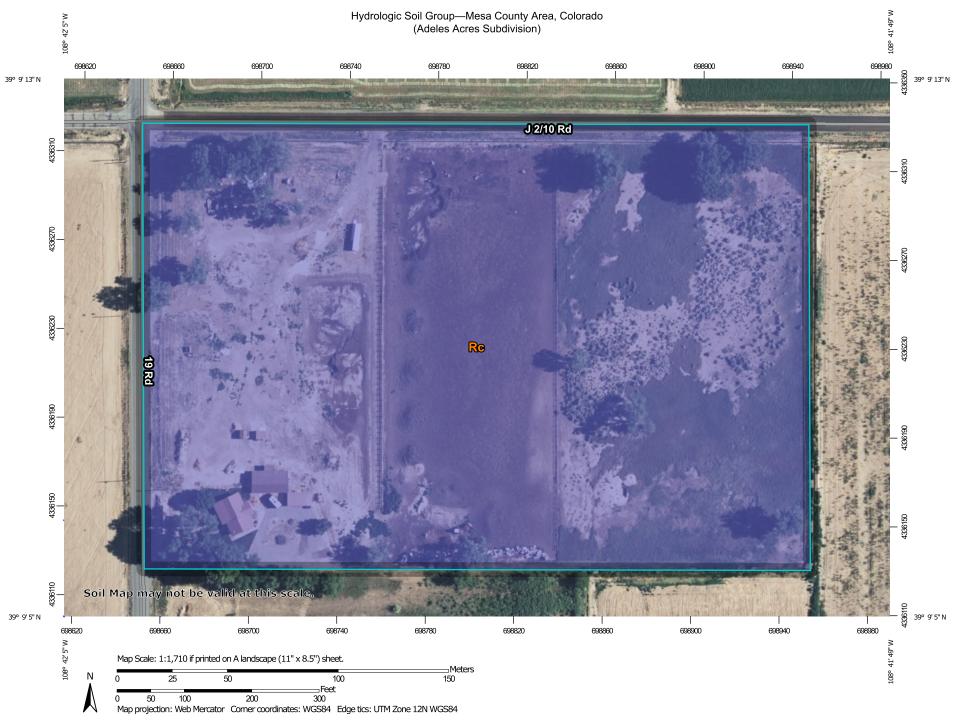
point selected by the user and does not represent

Digital Data Available

digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 10/31/2022 at 12:25 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24,000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil Water Features line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals В Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map С measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available Local Roads Maps from the Web Soil Survey are based on the Web Mercator 00 projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 13, Sep 6, 2022 C/D Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. D Not rated or not available Date(s) aerial images were photographed: Jun 24, 2020—Jul 8. 2020 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. В B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI	
Rc	Fruitland sandy clay loam, 0 to 2 percent slopes	В	15.0	100.0%	
Totals for Area of Interest			15.0	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

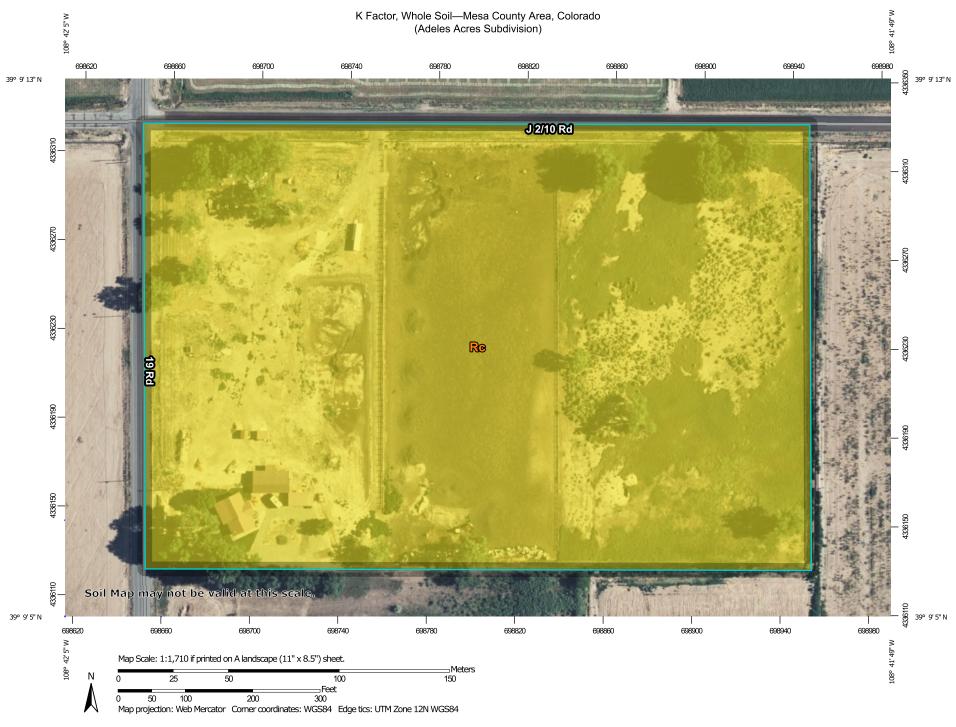
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

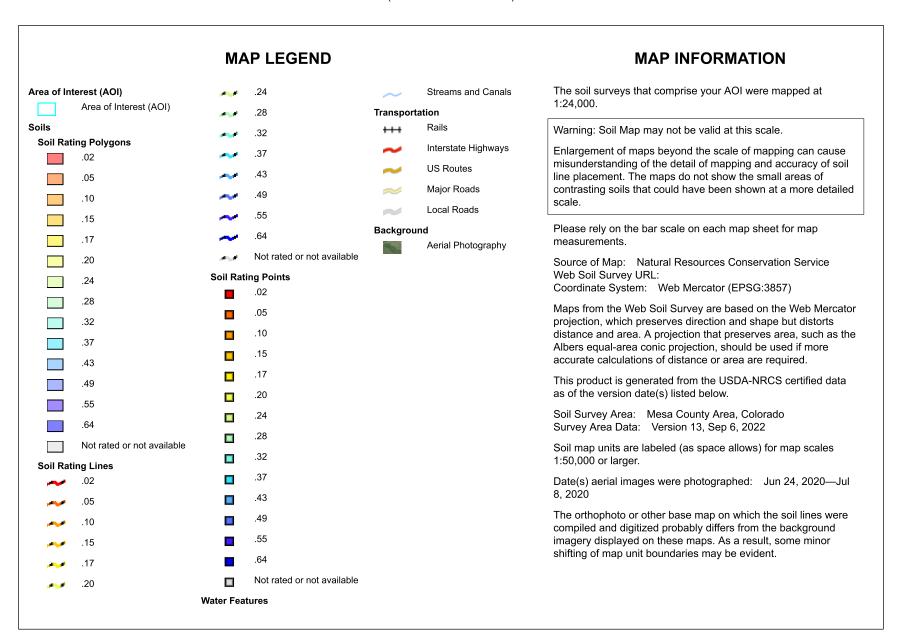
Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher





K Factor, Whole Soil

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI			
Rc	Fruitland sandy clay loam, 0 to 2 percent slopes	.17	15.0	100.0%			
Totals for Area of Interest			15.0	100.0%			

Description

Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and saturated hydraulic conductivity (Ksat). Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

"Erosion factor Kw (whole soil)" indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Factor K does not apply to organic horizons and is not reported for those layers.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Layer Options (Horizon Aggregation Method): Surface Layer (Not applicable)



NOAA Atlas 14, Volume 8, Version 2 Location name: Fruita, Colorado, USA* Latitude: 39.1525°, Longitude: -108.6993° Elevation: 4549.09 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹								nes) ¹	
Duration	Average recurrence interval (years)									
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.115 (0.093-0.148)	0.148 (0.120-0.191)	0.208 (0.167-0.269)	0.262 (0.209-0.340)	0.343 (0.266-0.473)	0.411 (0.309-0.573)	0.484 (0.349-0.693)	0.562 (0.386-0.832)	0.674 (0.442-1.03)	0.764 (0.484-1.18)
10-min	0.169 (0.137-0.217)	0.217 (0.176-0.280)	0.304 (0.245-0.393)	0.383 (0.306-0.498)	0.502 (0.389-0.692)	0.601 (0.452-0.839)	0.708 (0.511-1.02)	0.823 (0.565-1.22)	0.987 (0.647-1.50)	1.12 (0.709-1.72)
15-min	0.206 (0.167-0.265)	0.265 (0.214-0.342)	0.371 (0.299-0.480)	0.467 (0.374-0.607)	0.612 (0.475-0.844)	0.733 (0.551-1.02)	0.863 (0.623-1.24)	1.00 (0.689-1.48)	1.20 (0.789-1.84)	1.36 (0.864-2.10)
30-min	0.287 (0.232-0.369)	0.372 (0.301-0.480)	0.519 (0.418-0.671)	0.648 (0.518-0.842)	0.834 (0.643-1.14)	0.986 (0.738-1.37)	1.14 (0.822-1.63)	1.31 (0.897-1.93)	1.54 (1.01-2.34)	1.73 (1.09-2.66)
60-min	0.375 (0.303-0.482)	0.468 (0.378-0.603)	0.627 (0.505-0.811)	0.767 (0.613-0.996)	0.970 (0.748-1.32)	1.13 (0.850-1.57)	1.31 (0.939-1.86)	1.49 (1.02-2.19)	1.74 (1.14-2.64)	1.94 (1.23-2.98)
2-hr	0.463 (0.379-0.586)	0.563 (0.461-0.714)	0.735 (0.599-0.936)	0.886 (0.717-1.13)	1.10 (0.863-1.48)	1.28 (0.973-1.75)	1.47 (1.07-2.06)	1.66 (1.16-2.41)	1.94 (1.28-2.89)	2.15 (1.38-3.26)
3-hr	0.522 (0.431-0.656)	0.616 (0.507-0.774)	0.779 (0.639-0.982)	0.923 (0.753-1.17)	1.14 (0.897-1.51)	1.31 (1.00-1.77)	1.50 (1.10-2.08)	1.70 (1.19-2.44)	1.97 (1.32-2.93)	2.20 (1.42-3.30)
6-hr	0.636 (0.532-0.787)	0.726 (0.606-0.899)	0.885 (0.736-1.10)	1.03 (0.848-1.28)	1.24 (0.990-1.62)	1.41 (1.10-1.88)	1.60 (1.19-2.19)	1.80 (1.28-2.54)	2.08 (1.41-3.03)	2.30 (1.51-3.40)
12-hr	0.761 (0.644-0.926)	0.873 (0.737-1.06)	1.07 (0.897-1.30)	1.24 (1.03-1.52)	1.48 (1.20-1.91)	1.69 (1.32-2.20)	1.90 (1.43-2.55)	2.12 (1.53-2.95)	2.44 (1.68-3.49)	2.69 (1.79-3.91)
24-hr	0.894 (0.766-1.07)	1.03 (0.884-1.24)	1.27 (1.08-1.53)	1.48 (1.25-1.78)	1.78 (1.45-2.25)	2.02 (1.61-2.60)	2.28 (1.74-3.01)	2.55 (1.86-3.47)	2.92 (2.04-4.11)	3.22 (2.17-4.60)
2-day	1.03 (0.896-1.22)	1.19 (1.03-1.40)	1.45 (1.26-1.72)	1.69 (1.45-2.01)	2.04 (1.69-2.54)	2.32 (1.87-2.94)	2.62 (2.03-3.41)	2.94 (2.17-3.95)	3.38 (2.39-4.69)	3.74 (2.56-5.25)
3-day	1.11 (0.974-1.30)	1.28 (1.12-1.50)	1.58 (1.37-1.85)	1.84 (1.59-2.16)	2.21 (1.85-2.73)	2.52 (2.05-3.16)	2.85 (2.23-3.67)	3.19 (2.38-4.24)	3.67 (2.62-5.04)	4.05 (2.80-5.64)
4-day	1.18 (1.04-1.37)	1.36 (1.19-1.58)	1.67 (1.46-1.94)	1.94 (1.69-2.27)	2.34 (1.97-2.86)	2.66 (2.18-3.30)	3.00 (2.36-3.83)	3.35 (2.51-4.42)	3.85 (2.76-5.24)	4.24 (2.95-5.85)
7-day	1.34 (1.20-1.54)	1.54 (1.37-1.76)	1.87 (1.65-2.15)	2.16 (1.89-2.49)	2.57 (2.18-3.09)	2.90 (2.39-3.54)	3.24 (2.58-4.08)	3.60 (2.73-4.68)	4.10 (2.97-5.49)	4.48 (3.15-6.11)
10-day	1.49 (1.33-1.69)	1.69 (1.51-1.92)	2.04 (1.81-2.32)	2.33 (2.06-2.67)	2.75 (2.35-3.28)	3.09 (2.57-3.74)	3.44 (2.75-4.28)	3.80 (2.90-4.88)	4.29 (3.14-5.70)	4.68 (3.32-6.32)
20-day	1.89 (1.72-2.11)	2.14 (1.94-2.38)	2.54 (2.29-2.84)	2.88 (2.58-3.24)	3.36 (2.90-3.92)	3.74 (3.15-4.43)	4.12 (3.34-5.02)	4.51 (3.49-5.68)	5.03 (3.73-6.55)	5.44 (3.91-7.20)
30-day	2.23 (2.04-2.46)	2.52 (2.30-2.78)	2.99 (2.72-3.31)	3.38 (3.05-3.76)	3.91 (3.41-4.50)	4.33 (3.67-5.07)	4.74 (3.87-5.71)	5.16 (4.02-6.42)	5.71 (4.27-7.34)	6.13 (4.45-8.04)
45-day	2.66 (2.45-2.90)	3.01 (2.77-3.29)	3.58 (3.28-3.92)	4.03 (3.68-4.44)	4.65 (4.07-5.28)	5.11 (4.37-5.91)	5.56 (4.58-6.62)	6.01 (4.72-7.38)	6.58 (4.96-8.35)	7.00 (5.13-9.09)
60-day	3.03 (2.81-3.28)	3.44 (3.19-3.74)	4.09 (3.78-4.46)	4.61 (4.23-5.04)	5.30 (4.66-5.95)	5.80 (4.98-6.64)	6.28 (5.19-7.39)	6.74 (5.32-8.20)	7.32 (5.54-9.20)	7.74 (5.71-9.96)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

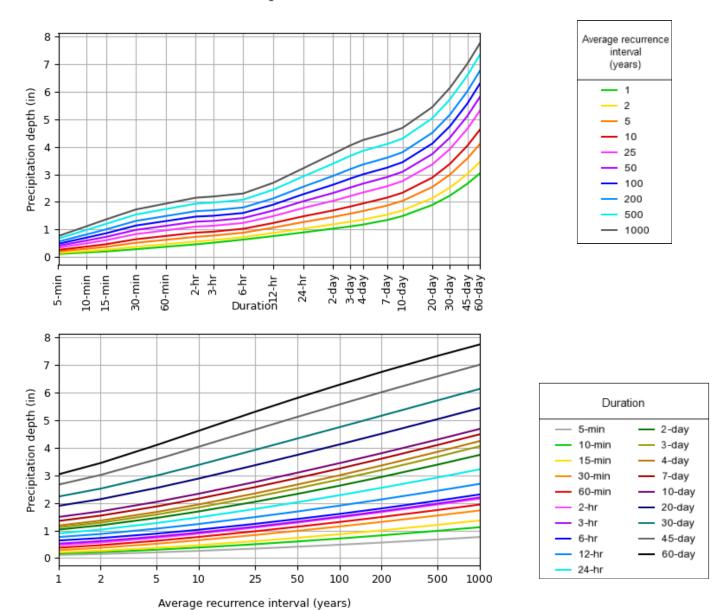
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 39.1525°, Longitude: -108.6993°



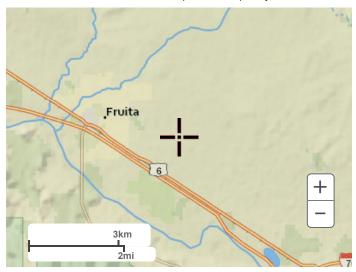
NOAA Atlas 14, Volume 8, Version 2

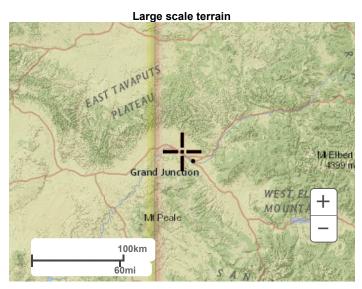
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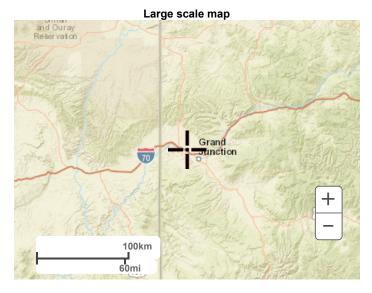
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Maps & aerials

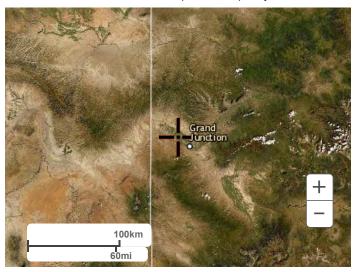
Small scale terrain







Large scale aerial



Back to Top

US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

Disclaimer

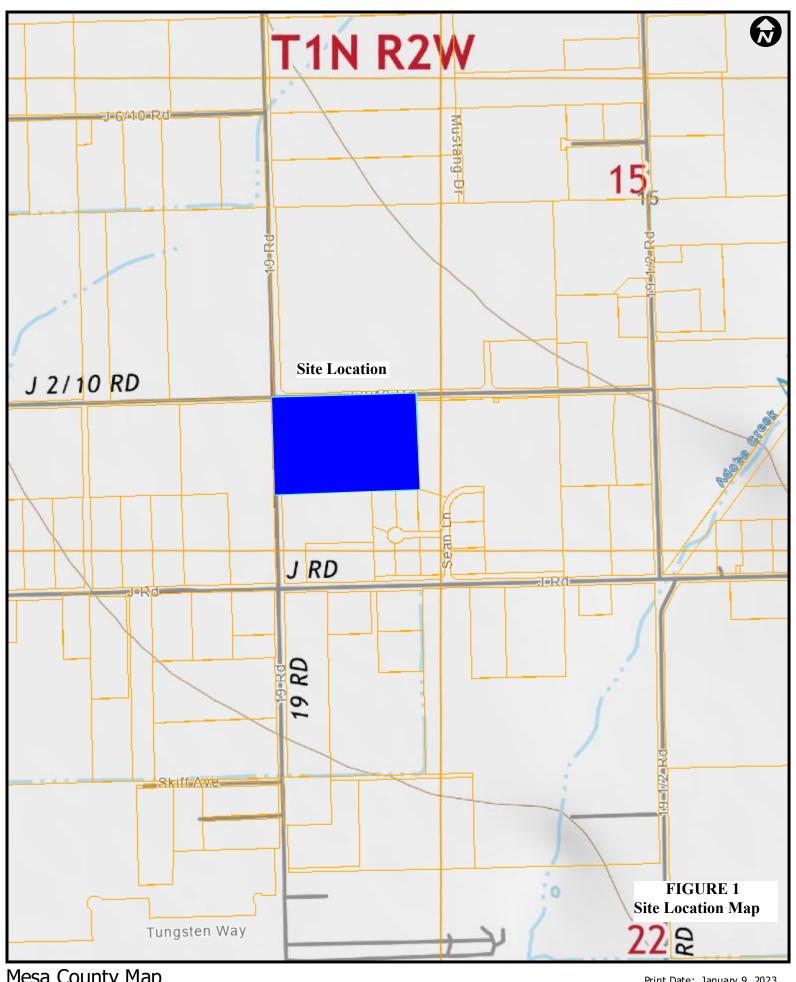


GEOTECHNICAL AND GEOLOGIC HAZARDS INVESTIGATION 1024 19 ROAD FRUITA, COLORADO PROJECT#02594-0001

DARRELL CORDOVA PO BOX 2227 GLENWOOD SPRINGS, COLORADO 81602

JANUARY 12, 2023

Huddleston-Berry Engineering and Testing, LLC 2789 Riverside Parkway Grand Junction, Colorado 81501



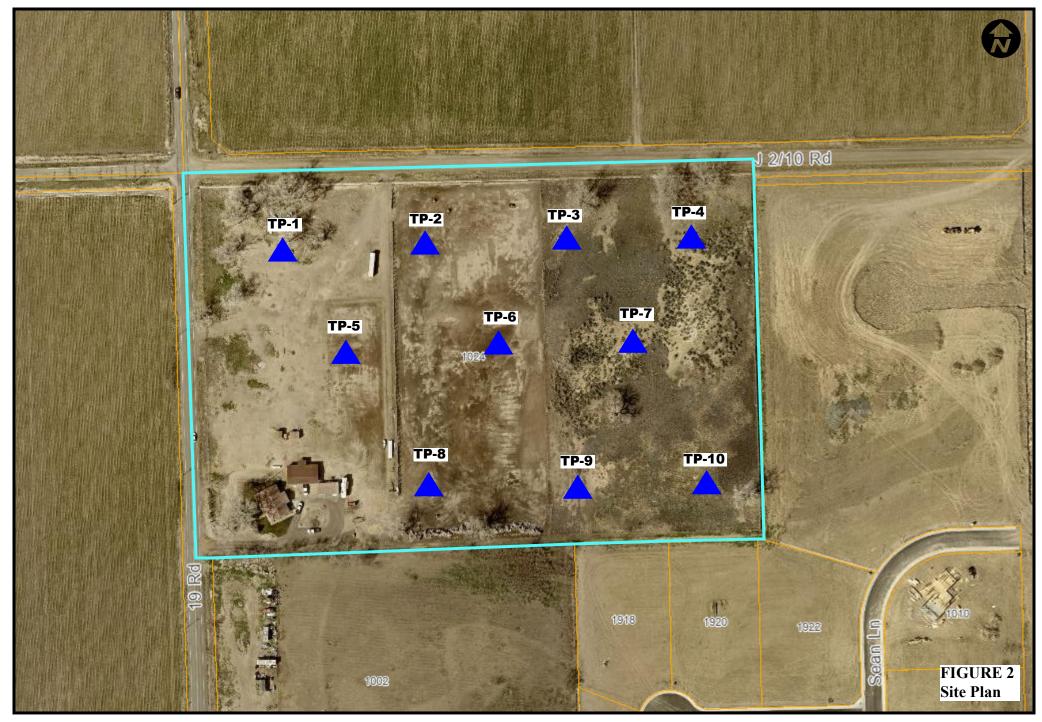
Mesa County Map

The Gographic Information System (GIS) and its components are designed as a source of reference for answering inquiries, for planning and for modeling GIS is not intended or does not repixe legal description information in the chain of title and other information crutained in diffical government records such as the County Clerk and Recorders office or the courts. In addition, the representations of location in this GIS cannot be substitute for actual legal surveys.

The information contained herein is believed accusted and suilable for the limited uses, and subject to the limitations, set forth above. Mesa County makes no warranty as to the accusery or suitability of any information contained herein. Users assume all risk and responsibility for any and all damages, including consequential damages, which may flow from the user's use of this information.

0.05 0.1 0.2 mi 0.075 0.15 0.3 km

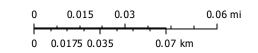
Print Date: January 9, 2023 Mesa County, Colorado **GIS/IT Department**



Mesa County Map

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The information contained herein is believed accusate and suitable for the limited uses, and subject to the limitations, set forth above. Mesa County mixes now warratly as to the accusacy or suitability of any information contained herein. Users assume all risk and responsibility for any and all damages, including consequential damages, which may flow from the user's use of this information.





TEST PIT NUMBER TP-1 PAGE 1 OF 1

Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005

PROJECT NAME 1024 19 Road **CLIENT** Darrell Cordova PROJECT NUMBER 02594-0001 PROJECT LOCATION Fruita, CO **COMPLETED** 12/19/22 **DATE STARTED** 12/19/22 GROUND ELEVATION **TEST PIT SIZE** EXCAVATION CONTRACTOR Wiseland **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF EXCAVATION 8.0 ft **EXCAVATION METHOD** Trackh/Backhoe **TAT END OF EXCAVATION** 8.0 ft LOGGED BY TC CHECKED BY MAB NOTES AFTER EXCAVATION _---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER POCKET PEN. (tsf) MOISTURE CONTENT (%) LIMITS GRAPHIC LOG BLOW COUNTS (N VALUE) RECOVERY (RQD) PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy SILT with organics (TOPSOIL) 11. 1.1, Sandy SILT (ml), tan and brown, moist to wet, medium dense to 2.5 **Walls Collapsing below 2' **Hit electrical line running from house northward to internet tower 5.0 GEOTECH BH COLUMNS 02594-0001 1024 19 RD.GPJ GINT US LAB.GDT 1/12/23 7.5 Bottom of test pit at 8.0 feet.

TEST PIT NUMBER TP-5 PAGE 1 OF 1

Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005

GEOTECH BH COLUMNS 02594-0001 1024 19 RD.GPJ GINT US LAB.GDT 1/12/23

CLIENT Darrell Cordova F			PROJECT NAME 1024 19 Road										
PROJECT NUMBER 02594-0001													
DATE	STAF	RTED 12/19/22 COMPLETED 12/19/22 G	GROUND ELEVATION TEST PIT SIZE										
EXCA	VATIO	ON CONTRACTOR Wiseland G											
EXCA	VATIO	ON METHOD Trackh/Backhoe	_										
LOGG	ED B	Y TC CHECKED BY MAB	_										
NOTE	s		AF	TER EXC	AVAT	ION							
				Й	%		j	Ή.	6)	ATT	ERBE IMITS	RG	NT
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	ASTIC IMIT	PLASTICITY INDEX	FINES CONTENT (%)
0.0				SAI	묎	_ =	PO	DR	≥ 0		PL	ا ځ څ	E I
0.0	<u>7</u> 1 1 _N	Sandy SILT with organics (TOPSOIL)										_	
	17. 7.17												
		Sandy SILT (ml), tan and brown, moist to wet, loose											
		**Walls Collapsing below 2'											
2.5													
5.0													
7.5													
		▼											
		Bottom of test pit at 8.0 feet.											

APPENDIX B

Hydrologic Calculations

- 1. Impervious Calculations Existing Conditions
- 2. Rational Method Calculations Existing Conditions
- 3. Impervious Calculations Developed Conditions
- 4. Rational Method Calculations Developed Conditions

PROJECT: Adeles Acres JOB NO.: 2060-001 CALC. BY: CTR

DATE:



Impervious Percentages - from Urban Drainage Table 6-3

Asphalt	100%
Gravel	40%
Drive & Walks	90%
Roofs	90%

Landscape	2%
Land Use 6	0%
Land Use 7	0%
Land Use 8	0%

SOIL TYPE:

В

(use equation from Table 6-4)



COMPOSITE IMPERVIOUSNESS

		Weigh	eighted Impervious and C Values			ues Areas (ac)								
Basin	Area (ac)	lmp.	C ₂	C ₅	C ₁₀	C ₁₀₀	Asphalt	Gravel	Drive & Walks	Roofs	Landscape	Land Use 6	Land Use 7	Land Use 8
EC-01	14.55	5.5%	0.03	0.04	0.10	0.45	0.21	0.40	0.03	0.13	13.77			
EC-02	0.72	24.5%	0.16	0.19	0.26	0.54	0.00	0.25	0.08	0.00	0.40			
									<u> </u>					
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Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	Kirpich
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	YES

Analysis Options

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:00:30	days hh:mm:ss
Reporting Time Step	0 00:00:30	days hh:mm:ss
Routing Time Step	5	seconds

Rainfall Details

Subbasin Summary

SN Subbasin	Area	Weighted	Average	Flow	Total	Total	Total	Peak	Time of
ID		Runoff	Slope	Length	Rainfall	Runoff	Runoff	Runoff	Concentration
		Coefficient					Volume		
	(ac)		(%)	(ft)	(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 EX-01	(ac)	0.0800	()	(ft) 1591.00	(in) 0.76	(in) 0.06	(ac-in) 0.89	(cfs) 0.94	(days hh:mm:ss) 0 00:56:10

Subbasin Hydrology

Subbasin: EX-01

Input Data

Area (ac)	14.55
Weighted Runoff Coefficient	80.0
Average Slope (%)	0.2
Flow Length (ft)	1591

Runoff Coefficient

	Area	2011	KUNON
Soil/Surface Description	(acres)	Group	Coeff.
Open Space, less than 25 years	14.55	B (0-2%)	0.08
Composite Area & Weighted Runoff Coeff.	14.55		0.08

Time of Concentration

TOC Method : Kirpich

Sheet Flow Equation :

Tc = (0.0078 * ((Lf^0.77) * (Sf^-0.385)))

Where:

Tc = Time of Concentration (min)

Lf = Flow Length (ft)

Sf = Slope (ft/ft)

User-Defined TOC override (minutes): 56.17

Total Rainfall (in)	0.76
Total Runoff (in)	0.06
Peak Runoff (cfs)	0.94
Rainfall Intensity	0.81
Weighted Runoff Coefficient	80.0
Time of Concentration (days hh:mm:ss)	0.00:56:10

Subbasin: EX-02

Input Data

Area (ac)	0.72
Weighted Runoff Coefficient	0.37
Average Slope (%)	0.5
Flow Length (ft)	967

Runoff Coefficient

	Area	Soil	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
Open Space, less than 25 years	0.39	B (0-2%)	0.08
Streets, less than 25 years	0.33	B (0-2%)	0.71
Composite Area & Weighted Runoff Coeff.	0.72		0.37

Time of Concentration

User-Defined TOC override (minutes): 17.11

Total Rainfall (in)	0.47
Total Runoff (in)	0.17
Peak Runoff (cfs)	0.44
Rainfall Intensity	1.634
Weighted Runoff Coefficient	0.37
Time of Concentration (days hh:mm:ss)	0 00:17:07

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	Kirpich
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	YES

Analysis Options

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:00:30	days hh:mm:ss
Reporting Time Step	0 00:00:30	days hh:mm:ss
Routing Time Step	5	seconds

Rainfall Details

Subbasin Summary

SN Subbasin	Area	Weighted	Average	Flow	Total	Total	Total	Peak	Time of
ID		Runoff	Slope	Length	Rainfall	Runoff	Runoff	Runoff	Concentration
		Coefficient					Volume		
				(6.)				(()	
	(ac)		(%)	(ft)	(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 EC-01	(ac) 14.55	0.0300	0.2000	(ft) 1591.00	(in) 0.46	(in) 0.01	(ac-in) 0.20	(cfs) 0.22	0 00:56:10

Subbasin Hydrology

Subbasin: EC-01

Input Data

Area (ac)	14.55
Weighted Runoff Coefficient	0.03
Average Slope (%)	0.2
Flow Length (ft)	1591

Runoff Coefficient

	Area	2011	RUHOH
Soil/Surface Description	(acres)	Group	Coeff.
Open Space, less than 25 years	14.55	B (0-2%)	0.03
Composite Area & Weighted Runoff Coeff.	14.55		0.03

Time of Concentration

TOC Method : Kirpich

Sheet Flow Equation :

Tc = (0.0078 * ((Lf^0.77) * (Sf^-0.385)))

Where:

Tc = Time of Concentration (min)

Lf = Flow Length (ft)

Sf = Slope (ft/ft)

User-Defined TOC override (minutes): 56.17

Total Rainfall (in)	0.46
Total Runoff (in)	0.01
Peak Runoff (cfs)	0.22
Rainfall Intensity	0.494
Weighted Runoff Coefficient	0.03
Time of Concentration (days hh:mm:ss)	0 00:56:10

Input Data

Area (ac)	0.72
Weighted Runoff Coefficient	0.16
Average Slope (%)	0.5
Flow Length (ft)	967

Runoff Coefficient

	Area	Soil	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
Open Space, less than 25 years	0.39	B (0-2%)	0.03
Streets, less than 25 years	0.33	B (0-2%)	0.32
Composite Area & Weighted Runoff Coeff.	0.72		0.16

Time of Concentration

User-Defined TOC override (minutes): 17.11

Total Rainfall (in)	0.29
Total Runoff (in)	0.05
Peak Runoff (cfs)	0.12
Rainfall Intensity	0.997
Weighted Runoff Coefficient	0.16
Time of Concentration (days hh:mm:ss)	0 00:17:07

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	Kirpich
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	YES

Analysis Options

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:00:30	days hh:mm:ss
Reporting Time Step	0 00:00:30	days hh:mm:ss
Routing Time Step	5	seconds

Rainfall Details

Subbasin Summary

SN Subbasin Area		Weighted	Average	Flow	Total	Total	Total	Peak	Time of
ID	ID		Slope	Length	Rainfall	Runoff	Runoff	Runoff	Concentration
		Coefficient					Volume		
	(ac)		(%)	(ft)	(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 EX-01	(ac)	0.1400	()	(ft) 1591.00	(in) 1.30	(in) 0.18	(ac-in) 2.63	(cfs) 2.82	(days hh:mm:ss) 0 00:56:10

Subbasin Hydrology

Subbasin: EX-01

Input Data

Area (as)	1155
Area (ac)	14.55
Weighted Runoff Coefficient	0.14
Average Slope (%)	0.2
Flow Length (ft)	1591

Runoff Coefficient

	Area	2011	Runon
Soil/Surface Description	(acres)	Group	Coeff.
Open Space, 25 years or greater	14.55	B (0-2%)	0.14
Composite Area & Weighted Runoff Coeff.	14.55		0.14

Time of Concentration

TOC Method : Kirpich

Sheet Flow Equation :

Tc = (0.0078 * ((Lf^0.77) * (Sf^-0.385)))

Where:

Tc = Time of Concentration (min)

Lf = Flow Length (ft)

Sf = Slope (ft/ft)

User-Defined TOC override (minutes): 56.17

Total Rainfall (in)	1.3
Total Runoff (in)	0.18
Peak Runoff (cfs)	2.82
Rainfall Intensity	1.384
Weighted Runoff Coefficient	0.14
Time of Concentration (days hh:mm:ss)	0 00:56:10

Subbasin: EX-02

Input Data

Area (ac)	0.72
Weighted Runoff Coefficient	0.44
Average Slope (%)	0.5
Flow Length (ft)	967

Runoff Coefficient

	Area	2011	RUHOH
Soil/Surface Description	(acres)	Group	Coeff.
Open Space, 25 years or greater	0.39	B (0-2%)	0.14
Streets, 25 years or greater	0.33	B (0-2%)	8.0
Composite Area & Weighted Runoff Coeff.	0.72		0.44

Time of Concentration

User-Defined TOC override (minutes): 17.11

Total Rainfall (in)	0.8
Total Runoff (in)	0.35
Peak Runoff (cfs)	0.89
Rainfall Intensity	2.79
Weighted Runoff Coefficient	0.44
Time of Concentration (days hh:mm:ss)	0 00:17:07

PROJECT: Adeles Acres JOB NO.: 2060-001 CALC. BY: CTR

DATE:



Impervious Percentages - from Urban Drainage Table 6-3

Asphalt	100%
Gravel	40%
Drive & Walks	90%
Roofs	90%

2%
0%
0%
0%

SOIL TYPE:

В

(use equation from Table 6-4)



COMPOSITE IMPERVIOUSNESS

		Weighted Impervious and C Values					Areas (ac)							
Basin	Area (ac)	Imp.	C ₂	C ₅	C ₁₀	C ₁₀₀	Asphalt	Gravel	Drive & Walks	Roofs	Landscape	Land Use 6	Land Use 7	Land Use 8
DC-01	7.35	60.5%	0.47	0.50	0.5470	0.71	1.11	0.00	0.90	2.75	2.58			
DC-02	2.05	65.7%	0.51	0.54	0.59	0.73	0.38	0.00	0.26	0.80	0.61			
DC-03	1.56	54.5%	0.41	0.44	0.50	0.68	0.19	0.00	0.11	0.61	0.65			
DC-04	0.98	9.2%	0.05	0.06	0.13	0.47	0.00	0.00	0.08	0.00	0.90			
DC-05	2.62	20.2%	0.13	0.15	0.22	0.52	0.18	0.45	0.03	0.13	1.84			
DC-06	0.75	19.0%	0.12	0.14	0.21	0.52	0.03	0.26	0.00	0.00	0.46			
Pond	11.93	56.4%	0.43	0.46	0.51	0.69	1.68	0.00	1.35	4.16	4.74			

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	User-Defined
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	YES

Analysis Options

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:00:30	days hh:mm:ss
Reporting Time Step	0 00:00:30	days hh:mm:ss
Routing Time Step	5	seconds

Rainfall Details

Subbasin Summary

Time of	Peak	Total	Total	Total	Weighted	Area	SN Subbasin
					3	/ ii Cu	
Concentration	Runoff	Runoff	Runoff	Rainfall	Runoff		ID
		Volume			Coefficient		
(days hh:mm:ss)	(cfs)	(ac-in)	(in)	(in)		(ac)	
0 00:16:52	14.66	4.12	0.56	0.79	0.7100	7.35	1 DC-01
0 00:13:40	4.64	1.06	0.52	0.71	0.7300	2.05	2 DC-02
0 00:09:59	3.76	0.63	0.40	0.59	0.6800	1.56	3 DC-03
0 00:11:32	1.54	0.29	0.30	0.64	0.4700	0.98	4 DC-04
0 00:28:07	2.91	1.37	0.52	1.00	0.5200	2.62	5 DC-05
0 00:16:36	1.10	0.31	0.41	0.79	0.5200	0.75	6 DC-06

Subbasin Hydrology

Subbasin: DC-01

Input Data

 Area (ac)
 7.35

 Weighted Runoff Coefficient
 0.71

Runoff Coefficient

	Area	Soil	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
-	5.21	-	0.71
Composite Area & Weighted Runoff Coeff.	5.21		0.71

Total Rainfall (in)	0.79
Total Runoff (in)	0.56
Peak Runoff (cfs)	14.66
Rainfall Intensity	2.81
Weighted Runoff Coefficient	0.71
Time of Concentration (days hh:mm:ss)	0 00:16:52

Input Data

Area (ac)	2.05
Weighted Runoff Coefficient	0.73

Runoff Coefficient

	Area	2011	Runott
Soil/Surface Description	(acres)	Group	Coeff.
-	2.05	-	0.73
Composite Area & Weighted Runoff Coeff	2 05		0.73

Total Rainfall (in)	0.71
Total Runoff (in)	0.52
Peak Runoff (cfs)	4.64
Rainfall Intensity	3.104
Weighted Runoff Coefficient	0.73
Time of Concentration (days hh:mm:ss)	0 00:13:41

Input Data

Area (ac)	1.56
Weighted Runoff Coefficient	0.68

Runoff Coefficient

	Area	2011	RUHOH
Soil/Surface Description	(acres)	Group	Coeff.
-	1.56	-	0.68
Composite Area & Weighted Runoff Coeff.	1.56		0.68

Total Rainfall (in)	0.59
Total Runoff (in)	0.4
Peak Runoff (cfs)	3.76
Rainfall Intensity	3.545
Weighted Runoff Coefficient	0.68
Time of Concentration (days hh:mm:ss)	0 00:09:59

Input Data

Area (ac)	0.98
Weighted Runoff Coefficient	0.47

Runoff Coefficient

	Alea	3011	Kulloli
Soil/Surface Description	(acres)	Group	Coeff.
-	0.98	-	0.47
Composite Area & Weighted Runoff Coeff.	0.98		0.47

Total Rainfall (in)	0.64
Total Runoff (in)	0.3
Peak Runoff (cfs)	1.54
Rainfall Intensity	3.343
Weighted Runoff Coefficient	0.47
Time of Concentration (days hh:mm:ss)	0 00:11:32

Input Data

Area (ac)	2.62
Weighted Runoff Coefficient	0.52

Runoff Coefficient

	Area	2011	Runott
Soil/Surface Description	(acres)	Group	Coeff.
-	2.62	-	0.52
Composite Area & Weighted Runoff Coeff	2 62		0.52

Total Rainfall (in)	1
Total Runoff (in)	0.52
Peak Runoff (cfs)	2.91
Rainfall Intensity	2.134
Weighted Runoff Coefficient	0.52
Time of Concentration (days hh:mm:ss)	0 00:28:08

Input Data

Area (ac)	0.75
Weighted Runoff Coefficient	0.52

Runoff Coefficient

	Area	2011	Runott
Soil/Surface Description	(acres)	Group	Coeff.
-	0.75	-	0.52
Composite Area & Weighted Runoff Coeff.	0.75		0.52

Total Rainfall (in)	0.79
Total Runoff (in)	0.41
Peak Runoff (cfs)	1.1
Rainfall Intensity	2.832
Weighted Runoff Coefficient	0.52
Time of Concentration (days hh:mm:ss)	0 00:16:37

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	User-Defined
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	YES

Analysis Options

Start Analysis On	00:00:00	0:00:00
End Analysis On	00:00:00	0:00:00
Start Reporting On	00:00:00	0:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:00:30	days hh:mm:ss
Reporting Time Step	0 00:00:30	days hh:mm:ss
Routing Time Step	5	seconds

Rainfall Details

Subbasin Summary

SN Subbasir	n Area	Weighted	Total	Total	Total	Peak	Time of
ID		Runoff	Rainfall	Runoff	Runoff	Runoff	Concentration
		Coefficient			Volume		
	(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1 DC-01	7.35	0.5500	0.46	0.25	1.87	6.65	0 00:16:52
2 DC-02	2.05	0.5900	0.41	0.24	0.50	2.20	0 00:13:40
3 DC-03	1.56	0.5000	0.35	0.17	0.27	1.62	0 00:09:59
4 DC-04	0.98	0.1300	0.38	0.05	0.05	0.25	0 00:11:32
5 DC-05	2.62	0.2200	0.59	0.13	0.34	0.72	0 00:28:07
6 DC-06	0.75	0.2100	0.46	0.10	0.07	0.26	0 00:16:36

Subbasin Hydrology

Subbasin: DC-01

Input Data

Area (ac)	7.35
Weighted Runoff Coefficient	0.55

Runoff Coefficient

II OOCIIIGICIIL			
	Area	Soil	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
-	5.21	-	0.55
Composite Area & Weighted Runoff Coeff.	5.21		0.55

Total Rainfall (in)	0.46
Total Runoff (in)	0.25
Peak Runoff (cfs)	6.65
Rainfall Intensity	1.645
Weighted Runoff Coefficient	0.55
Time of Concentration (days hh-mm-ss)	0.00:16:52

Input Data

Area (ac)	2.05
Weighted Runoff Coefficient	0.59

Runoff Coefficient

	Area	2011	Runon
Soil/Surface Description	(acres)	Group	Coeff.
-	2.05	-	0.59
Composite Area & Weighted Runoff Coeff.	2.05		0.59

Total Rainfall (in)	0.41
Total Runoff (in)	0.24
Peak Runoff (cfs)	2.2
Rainfall Intensity	1.817
Weighted Runoff Coefficient	0.59
Time of Concentration (days hh:mm:ss)	0 00:13:41

Input Data

Area (ac)	1.56
Weighted Runoff Coefficient	0.5

Runoff Coefficient

	Area	2011	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
-	1.56	-	0.5
Composite Area & Weighted Runoff Coeff.	1.56		0.5

Total Rainfall (in)	0.35
Total Runoff (in)	0.17
Peak Runoff (cfs)	1.62
Rainfall Intensity	2.076
Weighted Runoff Coefficient	0.5
Time of Concentration (days hh:mm:ss)	0 00:09:59

Input Data

Area (ac)	0.98
Weighted Runoff Coefficient	0.13

Runoff Coefficient

	Alea	3011	RUHOH
Soil/Surface Description	(acres)	Group	Coeff.
-	0.98	-	0.13
Composite Area & Weighted Runoff Coeff.	0.98		0.13

Total Rainfall (in)	0.38
Total Runoff (in)	0.05
Peak Runoff (cfs)	0.25
Rainfall Intensity	1.958
Weighted Runoff Coefficient	0.13
Time of Concentration (days hh:mm:ss)	0 00:11:32

Input Data

Area (ac)	2.62
Weighted Runoff Coefficient	0 22

Runoff Coefficient

	Alea	3011	Kulloli
Soil/Surface Description	(acres)	Group	Coeff.
-	2.62	-	0.22
Composite Area & Weighted Runoff Coeff.	2.62		0.22

Total Rainfall (in)	0.59
Total Runoff (in)	0.13
Peak Runoff (cfs)	0.72
Rainfall Intensity	1.25
Weighted Runoff Coefficient	0.22
Time of Concentration (days hh:mm:ss)	0 00:28:08

Input Data

Area (ac)	0.75
Weighted Runoff Coefficient	0.21

Runoff Coefficient

	Area	2011	RUHOH
Soil/Surface Description	(acres) Group		
-	0.75	-	0.21
Composite Area & Weighted Runoff Coeff.	0.75		0.21

Total Rainfall (in)	0.46
Total Runoff (in)	0.1
Peak Runoff (cfs)	0.26
Rainfall Intensity	1.658
Weighted Runoff Coefficient	0.21
Time of Concentration (days hh:mm:ss)	0 00:16:37

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	Rational
Time of Concentration (TOC) Method	User-Defined
Link Routing Method	Hydrodynamic
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	YES

Analysis Options

Start Analysis On	 00:00:00	0:00:00
End Analysis On	 00:00:00	0:00:00
Start Reporting On	 00:00:00	0:00:00
Antecedent Dry Days	 0	days
Runoff (Dry Weather) Time Step	 0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	 0 00:00:30	days hh:mm:ss
Reporting Time Step	 0 00:00:30	days hh:mm:ss
Routing Time Step	 5	seconds

Rainfall Details

Subbasin Summary

Time of	Peak	Total	Total	Total	Weighted	Area	SN Subbasin
					3	711 00	
Concentration	Runoff	Runoff	Runoff	Rainfall	Runoff		ID
		Volume			Coefficient		
(days hh:mm:ss)	(cfs)	(ac-in)	(in)	(in)		(ac)	
0 00:16:52	3.47	0.97	0.13	0.28	0.4700	7.35	1 DC-01
0 00:13:40	1.16	0.26	0.13	0.25	0.5100	2.05	2 DC-02
0 00:09:59	0.81	0.14	0.09	0.21	0.4100	1.56	3 DC-03
0 00:11:32	0.06	0.01	0.01	0.23	0.0500	0.98	4 DC-04
0 00:28:07	0.26	0.12	0.05	0.36	0.1300	2.62	5 DC-05
0 00:16:36	0.09	0.03	0.03	0.28	0.1200	0.75	6 DC-06

Subbasin Hydrology

Subbasin: DC-01

Input Data

 Area (ac)
 7.35

 Weighted Runoff Coefficient
 0.47

Runoff Coefficient

	Area	Soil	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
-	5.21	-	0.47
Composite Area & Weighted Runoff Coeff.	5.21		0.47

Total Rainfall (in)	0.28
Total Runoff (in)	0.13
Peak Runoff (cfs)	3.47
Rainfall Intensity	1.004
Weighted Runoff Coefficient	0.47
Time of Concentration (days hh:mm:ss)	0 00:16:52

Input Data

Area (ac)	2.05
Weighted Runoff Coefficient	0.51

Runoff Coefficient

	Area	2011	Runott
Soil/Surface Description	(acres)	Group	Coeff.
-	2.05	-	0.51
Composite Area & Weighted Runoff Coeff	2 05		0.51

Total Rainfall (in)	0.25
Total Runoff (in)	0.13
Peak Runoff (cfs)	1.16
Rainfall Intensity	1.109
Weighted Runoff Coefficient	0.51
Time of Concentration (days hh:mm:ss)	0 00:13:41

Input Data

Area (ac)	1.56
Weighted Runoff Coefficient	0.41

Runoff Coefficient

	Area	2011	Runoff
Soil/Surface Description	(acres)	Group	Coeff.
-	1.56	-	0.41
Composite Area & Weighted Runoff Coeff.	1.56		0.41

Total Rainfall (in)	0.21
Total Runoff (in)	0.09
Peak Runoff (cfs)	0.81
Rainfall Intensity	1.267
Weighted Runoff Coefficient	0.41
Time of Concentration (days hh:mm:ss)	0 00:09:59

Input Data

Area (ac)	0.98
Weighted Runoff Coefficient	0.05

Runoff Coefficient

	Alea	3011	KUHOH
Soil/Surface Description	(acres)	Group	Coeff.
-	0.98	-	0.05
Composite Area & Weighted Runoff Coeff.	0.98		0.05

Total Rainfall (in)	0.23
Total Runoff (in)	0.01
Peak Runoff (cfs)	0.06
Rainfall Intensity	1.194
Weighted Runoff Coefficient	0.05
Time of Concentration (days hh:mm:ss)	0 00:11:32

Input Data

Area (ac)	2.62
Weighted Runoff Coefficient	0.13

Runoff Coefficient

	Area	2011	Runott
Soil/Surface Description	(acres)	Group	Coeff.
-	2.62	-	0.13
Composite Area & Weighted Runoff Coeff	2 62		0.13

Total Rainfall (in)	0.36
Total Runoff (in)	0.05
Peak Runoff (cfs)	0.26
Rainfall Intensity	0.762
Weighted Runoff Coefficient	0.13
Time of Concentration (days hh:mm:ss)	0 00:28:08

Input Data

Area (ac)	0.75
Weighted Runoff Coefficient	0.12

Runoff Coefficient

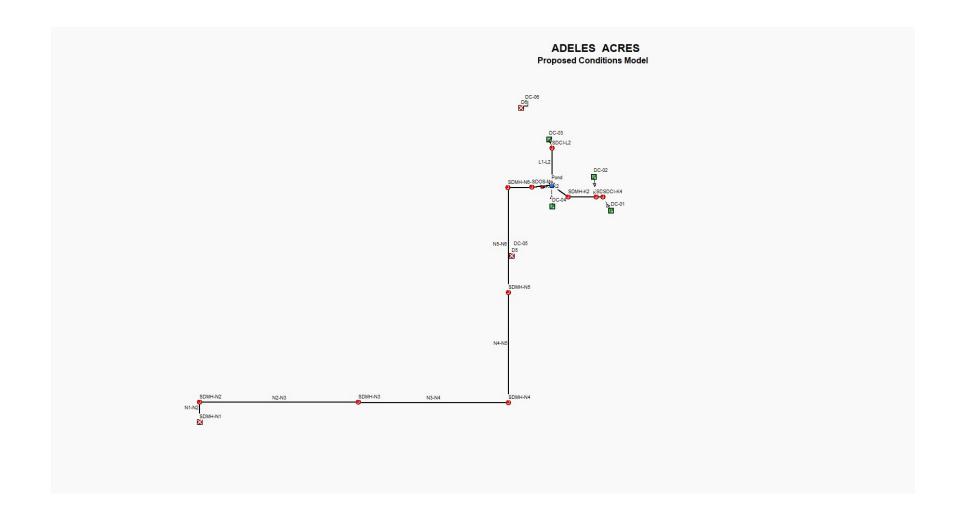
Агеа	2011	Runott
(acres)	Group	Coeff.
0.75	-	0.12
0.75		0.12
	(acres) 0.75	(acres) Group 0.75 -

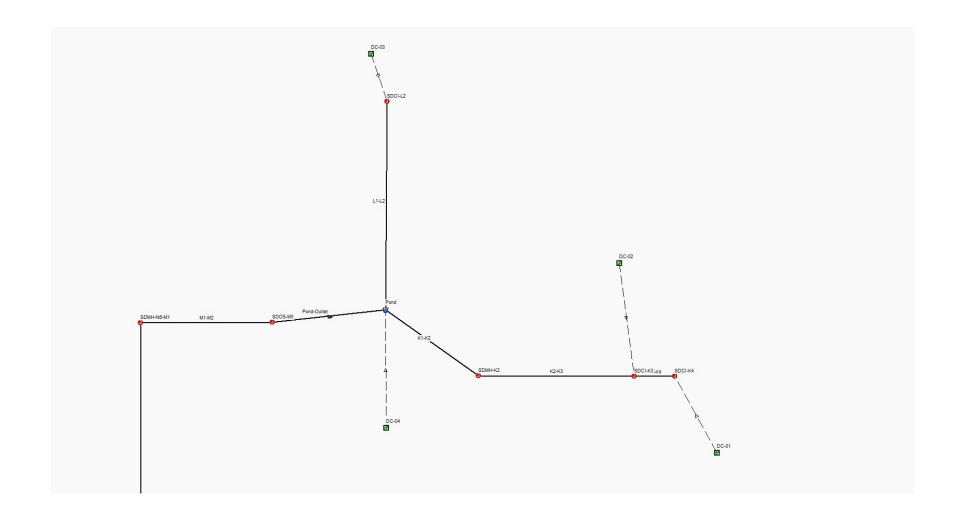
Total Rainfall (in)	0.28
Total Runoff (in)	0.03
Peak Runoff (cfs)	0.09
Rainfall Intensity	1.012
Weighted Runoff Coefficient	0.12
Time of Concentration (days hh:mm:ss)	0 00:16:37

APPENDIX C

Proposed Hydraulic Model Results

- 1. SSA Developed Conditions Model View(s)
- 2. 2-Year Design Storm
- 3. 10-Year Design Storm
- 4. 100-Year Design Storm
- 5. Profile Views of Proposed Storm Drain





```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.4.133 (Build 0)
******
Project Description
File Name ...... 2060-001 PR Model - Rational 2-YR.SPF
*****
Analysis Options
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... User-Defined
Return Period..... 2 years
Link Routing Method ..... Hydrodynamic
Storage Node Exfiltration.. Horton, wetted area
Starting Date ..... JUL-04-2017 00:00:00
Ending Date ..... JUL-08-2017 00:00:00
Report Time Step ..... 00:00:10
*****
Element Count
Number of subbasins ..... 6
Number of nodes ..... 14
Number of links ..... 11
Subbasin Summary
Subbasin
                Total
             7.35
2.05
DC-01
DC-02
DC-03
                 1.56
DC-04
                 0.98
                 2.62
DC-05
DC-06
                 0.75
*****
Node Summary
             Node
            Type
______
```

Pond	STO	ORAGE	4539.	16 4546.4	0.00		
************* Link Summary ********* Link ID	У	ode	To Node	Element Type	Lengtl ft	-	Manning's Roughness
K1-K2 K2-K3 K3-K4 L1-L2 M1-M2 N1-N2 N2-N3 N3-N4 N4-N5 N5-N6 Pond-Outlet	SDMH-K2 SDCI-K3 SDCI-K4 SDCI-L2 SDOS-M5 SDMH-N2 SDMH-N3 SDMH-N4 SDMH-N5 SDMH-N6 Pond	3 4 2 5 5 2 3 3 4 5	Pond SDMH-K2 SDCI-K3 Pond SDMH-N6-M1 SDMH-N1 SDMH-N2 SDMH-N3 SDMH-N4 SDMH-N5 SDOS-M5	CONDUIT	119.0 31.0 115.0 101.0 85.3 685.0 645.0	0.5042 0.4839 0.4957 0.3960 0.3986 0.3956 0.4000 0.3095	0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130
**************************************	on Summary						
Link Design	Shape		Depth/	Width	No. of	Cross	Full Flow
ID Flow			Diameter		Barrels	Sectional	Hydraulic
Capacity			5.	5.		Area	Radius
cfs			ft	ft		ft²	ft
K1-K2 16.00	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
K2-K3 16.06	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
K3-K4 15.74	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
L1-L2 7.40	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
M1-M2 6.61	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
N1-N2	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.63 N2-N3	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.61 N3-N4	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.64 N4-N5	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
5.84 N5-N6 5.85	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
************* Transect Sur ********	mmary ****						
Transect C&0 Area:		0 0007	0.0015	0 0007	0.0040		
	0.0002 0.0060 0.0323	0.0007 0.0087 0.0414	0.0015 0.0126 0.0519	0.0027 0.0179 0.0637	0.0042 0.0244 0.0767		

Soil/Surf	ace Descript	tion			Area (acres)	Soil Group	Runoff Coeff.
Subbasin							
_	Area & Weig	ghted Runof	f Coeff.		5.21 5.21	-	0.47 0.47
Soil/Surf	ace Descript	tion			Area (acres)	Soil Group	Runoff Coeff.
Subbasin	DC-01						
Runoff Co	************ efficient Co	omputations	Report				
	y Error (%)		0.001	3.330			
Initial S	Outflow tored Volume red Volume	e	0.126 0.000 0.000	0.041 0.000 0.000			
External	Inflow		0.000	0.000			
Flow Rout	************* ing Continu:	ity	Volume acre-ft	Volume Mgallons			
	cipitation y Error (%)		0.358 0.646	0.280			
Runoff Qu	************* antity Cont	inuity	Volume acre-ft	Depth inches			
	1.0000	1.0000	1.0000	1.0000	1.0000		
	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000		
	0.5415 1.0000	0.6133 1.0000	0.7100 1.0000	0.8067 1.0000	0.9033 1.0000		
	0.0121 0.0723 0.3069	0.0241 0.1193 0.3539	0.0362 0.1662 0.4008	0.0482 0.2131 0.4477	0.0603 0.2600 0.4946		
Width:	0.8958	0.9220	0.9481	0.9741	1.0000		
	0.4909 0.6284 0.7634	0.5186 0.6556 0.7901	0.5462 0.6827 0.8167	0.4331 0.5737 0.7097 0.8432	0.6011 0.7366 0.8696		
	0.1760 0.2076 0.3506	0.1828 0.2364 0.3789	0.1855 0.2651 0.4070	0.1911 0.2937 0.4351	0.1986 0.3222 0.4630		
Hrad:	0.0139 0.0834 0.1095	0.0278 0.0743 0.1222	0.0417 0.0783 0.1352	0.0556 0.0869 0.1486	0.0695 0.0976 0.1622		
II mad.	0.7506 0.8891	0.7783 0.9169	0.8060 0.9446	0.8337 0.9723	0.8614 1.0000		
	0.3349 0.4735 0.6120	0.3626 0.5012 0.6397	0.3903 0.5289 0.6674	0.4180 0.5566 0.6952	0.4457 0.5843 0.7229		
	0.0911 0.1963	0.1069	0.1252 0.2518	0.1463 0.2795	0.1700 0.3072		

- Composite Area	a & Weighted Runoff Coeff.					2.05	-	0.51 0.51
Subbasin DC-03								
Soil/Surface D						rea res)	Soil Group	Runoff Coeff.
- Composite Area	& Weighted Ru	noff Coe	eff.			1.56 1.56	-	0.41
Subbasin DC-04								
Soil/Surface D						rea res)	Soil Group	
- Composite Area	& Weighted Ru	noff Coe	eff.			0.98 0.98	-	0.05
Subbasin DC-05								
Soil/Surface D	escription					rea res)	Soil Group	Runoff Coeff.
- Composito Area	. Majahtad D	noff Cod				 2.62 2.62	<u>-</u> -	0.13 0.13
Composite Area		MOTI COE	:11.			2.02		0.13
Subbasin DC-06					7.		0-11	D a 5.5
Soil/Surface D	escription					rea res) 	Soil Group	Runoff Coeff.
- Composite Area	& Weighted Ru	ınoff Co∈	eff.			0.75 0.75	-	0.12 0.12
**************************************	f Summary							
 Subbasin	Accumulated	Rainf	 all	Total	 Peak	Weighted		Time of
ID	Precip in	Intens ir	ity /hr	Runoff in		Runoff Coeff		entration hh:mm:ss
DC-01 DC-02 DC-03 DC-04 DC-05 DC-06	0.28 0.25 0.21 0.23 0.36 0.28	1 1 1 0	.00 .11 .27 .19 .76	0.13 0.13 0.09 0.01 0.05 0.03		0.510 0.410 0.050 0.130	0 0 0	00:13:40

Node ID	Average Ma Depth Attained Att	Depth ained A	HGI ttained	occi l	urrence	Total Flooded Volume	Time Flooded	
	ft 	ft 	ft 	days	hh:mm	acre-in	minutes	hh:mm:ss

SDCI-K3	0.00	0.81	4541.48	0	00:17	0	0	0:00:00
SDCI-K4	0.00	0.85	4541.67	0	00:17	0	0	0:00:00
SDCI-L2	0.00	0.35	4541.60	0	00:10	0	0	0:00:00
SDMH-K2	0.07	0.83	4540.90	0	00:17	0	0	0:00:00
SDMH-N2	0.03	0.12	4530.72	0	01:06	0	0	0:00:00
SDMH-N3	0.03	0.12	4533.43	0	00:57	0	0	0:00:00
SDMH-N4	0.03	0.12	4536.01	0	00:47	0	0	0:00:00
SDMH-N5	0.03	0.13	4537.49	0	00:38	0	0	0:00:00
SDMH-N6-M1	0.03	0.12	4538.88	0	00:39	0	0	0:00:00
SDOS-M5	0.03	0.12	4539.28	0	00:34	0	0	0:00:00
D5	0.00	0.00	0.00	0	00:00	0	0	0:00:00
D6	0.00	0.00	0.00	0	00:00	0	0	0:00:00
SDMH-N1	0.03	0.11	4530.37	0	01:06	0	0	0:00:00
Pond	0.31	1.61	4540.77	0	00:34	0	0	0:00:00

Node ID	Element Type	Maximum Lateral Inflow cfs	Peak Inflow cfs	Peak Occu	lime of Inflow Irrence hh:mm	Flooding Overflow	
SDCI-K3 SDCI-K4 SDCI-L2 SDMH-K2 SDMH-N2 SDMH-N3 SDMH-N4 SDMH-N5 SDMH-N6-M1 SDOS-M5 D5	JUNCTION OUTFALL	1.16 3.47 0.81 0.00 0.00 0.00 0.00 0.00 0.00	4.34 3.47 0.81 4.33 0.08 0.08 0.08 0.08 0.08	0 0 0 0 0 0 0	00:17 00:16 00:10 00:17 01:01 00:51 00:43 00:39 00:35 00:34	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	
D6 SDMH-N1 Pond	OUTFALL OUTFALL STORAGE	0.09 0.00 0.06	0.09 0.08 4.61	0 0	00:16 01:06 00:17	0.00 0.00 0.00	

Storage Node Summary

-	ge Node ID Time of Max.	Maximum Total	- Maximum	Time of Max	Average	Average	Maximum
		Ponded	Ponded	Ponded	Ponded	Ponded	Storage Node
Exfiltra	ation Exfiltr	ration Exfiltr	ated				_
		Volume	Volume	Volume	Volume	Volume	Outflow
Rate	Rate	Volume					
		1000 ft ³	(%)	days hh:mm	1000 ft ³	(%)	cfs
cfm	hh:mm:ss	1000 ft ³					
Pond		4.718	- 5	0 00:34	0.575	1	0.17
0.00	0:00:00	0.000	9	0 00.54	0.373	_	0.17

Outfall Node ID	Flow	Average	Peak
	Frequency	Flow	Inflow
	(%)	cfs	cfs
D5	0.97	0.13	0.26
D6	0.57	0.05	0.09
SDMH-N1	31.88	0.05	0.08
System	11.14	0.22	0.29

Link Flow Summary ********

Link ID		Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of	ТС	tal Reported	D	1. 121	77-7	D l	4	7 3	26
Maximum	Тí	Type .me Condition	Pea	K F.TOM	Velocity	Factor	during	Flow	Maximum
ria zrimani		inc condicton	Occu	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharg	red		,		5. /		-	-	
Depth minu	1+29		days	hh:mm	ft/sec		cfs	cfs	Flow
Береп штпа		,							
K1 –K2		CONDUIT	0	00:17	3.86	1.00	4.31	16.00	0.27
0.43	0		Ü	00.17	3.00	1.00	1.01	10.00	0.27
K2-K3		CONDUIT	0	00:17	3.58	1.00	4.33	16.06	0.27
0.41 K3-K4	0	Calculated CONDUIT	0	00:17	2.82	1.00	3.46	15.74	0.22
0.41	0	Calculated	U	00.17	2.02	1.00	3.40	13.74	0.22
L1-L2		CONDUIT	0	00:10	2.63	1.00	0.78	7.40	0.11
0.23	0	Calculated	0	00:35	1.21	1.00	0.00	C C1	0 01
M1-M2 0.08	0	CONDUIT Calculated	0	00:35	1.21	1.00	0.08	6.61	0.01
N1-N2	O	CONDUIT	0	01:06	1.25	1.00	0.08	6.63	0.01
0.08	0	Calculated							
N2-N3 0.08	0	CONDUIT Calculated	0	01:01	1.28	1.00	0.08	6.61	0.01
N3-N4	U	CONDUIT	0	00:51	1.36	1.00	0.08	6.64	0.01
0.08	0	Calculated							
N4-N5 0.08	0	CONDUIT	0	00:43	1.19	1.00	0.08	5.84	0.01
0.08 N5-N6	U	Calculated CONDUIT	0	00:39	1.15	1.00	0.08	5.85	0.01
0.08	0	Calculated	,		0		2.00	2.00	
Pond-Outlet		OUTLET	0	00:34			0.08		

Link Pond-Outlet (3)

Analysis began on: Thu Mar 2 19:22:40 2023 Analysis ended on: Thu Mar 2 19:22:51 2023 Total elapsed time: 00:00:11

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.4.133 (Build 0)
******
Project Description
File Name ...... 2060-001 PR Model - Rational 10-YR.SPF
*****
Analysis Options
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... User-Defined
Return Period..... 10 years
Link Routing Method ..... Hydrodynamic
Storage Node Exfiltration.. Horton, wetted area
Starting Date ..... JUL-04-2017 00:00:00
Ending Date ..... JUL-08-2017 00:00:00
Report Time Step ..... 00:00:10
*****
Element Count
Number of subbasins ..... 6
Number of nodes ..... 14
Number of links ..... 11
Subbasin Summary
Subbasin
                Total
             7.35
2.05
DC-01
DC-02
DC-03
                 1.56
DC-04
                 0.98
                 2.62
DC-05
DC-06
                 0.75
*****
Node Summary
             Node
            Type
______
```

Pond	STO	ORAGE	4539.	16 4546.4	0.00		
************* Link Summary ********* Link ID	У	ode	To Node	Element Type	Lengtl ft	-	Manning's Roughness
K1-K2 K2-K3 K3-K4 L1-L2 M1-M2 N1-N2 N2-N3 N3-N4 N4-N5 N5-N6 Pond-Outlet	SDMH-K2 SDCI-K3 SDCI-K4 SDCI-L2 SDOS-M5 SDMH-N2 SDMH-N3 SDMH-N4 SDMH-N5 SDMH-N6 Pond	3 4 2 5 5 2 3 3 4 5	Pond SDMH-K2 SDCI-K3 Pond SDMH-N6-M1 SDMH-N1 SDMH-N2 SDMH-N3 SDMH-N4 SDMH-N5 SDOS-M5	CONDUIT	119.0 31.0 115.0 101.0 85.3 685.0 645.0	0.5042 0.4839 0.4957 0.3960 0.3986 0.3956 0.4000 0.3095	0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130
**************************************	on Summary						
Link Design	Shape		Depth/	Width	No. of	Cross	Full Flow
ID Flow			Diameter		Barrels	Sectional	Hydraulic
Capacity			5.	5.		Area	Radius
cfs			ft	ft		ft²	ft
K1-K2 16.00	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
K2-K3 16.06	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
K3-K4 15.74	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
L1-L2 7.40	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
M1-M2 6.61	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
N1-N2	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.63 N2-N3	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.61 N3-N4	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.64 N4-N5	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
5.84 N5-N6 5.85	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
************* Transect Sur ********	mmary ****						
Transect C&0 Area:		0 0007	0.0015	0 0007	0.0040		
	0.0002 0.0060 0.0323	0.0007 0.0087 0.0414	0.0015 0.0126 0.0519	0.0027 0.0179 0.0637	0.0042 0.0244 0.0767		

Soil/Surf	ace Descript	tion 			(acres)	Group	Coeff.
					Area	Soil	Runoff
 Subbasin	DC-02						
- Composite	e Area & Weig	ghted Runoi	ff Coeff.		5.21 5.21	-	0.55 0.55
Soil/Surf	ace Descript	tion			Area (acres)	Soil Group	Runoff Coeff.
					_		
 Subbasin	DC=01						
Runoff Co	*************** efficient Co	omputations	Report				
Continuit	ty Error (%)	••••	0.001				
Final Sto	red Volume		0.000	0.000			
	Outflow Stored Volume		0.255 0.000	0.083			
	**************************************		0.000	0.000			
Flow Rout	********** ing Continu:	ity	Volume acre-ft	Volume Mgallons			
	ecipitation by Error (%)		0.586 0.563	0.459			
	antity Cont		acre-ft	inches			
	****		Volume	Depth			
	1.0000	1.0000	1.0000	1.0000	1.0000		
	1.0000	1.0000	1.0000	1.0000	1.0000		
	1.0000	1.0000	1.0000	1.0000	1.0000		
	0.5415 1.0000	0.6133 1.0000	0.7100 1.0000	0.8067 1.0000	0.9033 1.0000		
	0.0723	0.1193 0.3539	0.1662 0.4008	0.2131	0.2600 0.4946		
Width:	0.0121	0.0241	0.0362	0.0482	0.0603		
	0.8958	0.9220	0.9481	0.9741	1.0000		
	0.6284	0.6556 0.7901	0.6827 0.8167	0.7097	0.7366 0.8696		
	0.3506 0.4909	0.3789 0.5186	0.4070 0.5462	0.4351 0.5737	0.4630 0.6011		
	0.1760 0.2076	0.1828 0.2364	0.1855 0.2651	0.1911 0.2937	0.1986 0.3222		
	0.1095	0.1222	0.1352	0.1486	0.1622		
	0.0139 0.0834	0.0278 0.0743	0.0417 0.0783	0.0556 0.0869	0.0695 0.0976		
Hrad:	0.8891	0.9169	0.9446	0.9723	1.0000		
	0.6120 0.7506	0.6397 0.7783	0.6674 0.8060	0.6952 0.8337	0.7229 0.8614		
	0.3349 0.4735	0.3626 0.5012	0.3903 0.5289	0.4180 0.5566	0.4457 0.5843		
	0.1963	0.2240	0.2518	0.2795	0.3072		
	0.0911	0.1069	0.1252	0.1463	0.1700		

- Composite Area	& Weighted	Runoff C	Coeff.			2.05 2.05	-	0.59 0.59
Subbasin DC-03								
Soil/Surface De	escription					rea res)	Soil Group	Runoff Coeff.
- Composite Area	& Weighted	Runoff C	Coeff.			1.56 1.56	-	0.50 0.50
Subbasin DC-04								
Soil/Surface De						rea res)	Soil Group	
- Composite Area	& Weighted	Runoff C	Coeff.			0.98 0.98	-	0.13 0.13
Subbasin DC-05								
Soil/Surface De	escription					rea res) 	Soil Group	Runoff Coeff.
- Composite Area	& Weighted	Runoff C	Coeff.			2.62 2.62	-	0.22 0.22
Subbasin DC-06								
Soil/Surface De	escription					rea res) 	Soil Group	Runoff Coeff.
- Composite Area	& Weighted	Runoff C	Coeff.			0.75 0.75	-	0.21 0.21
**************************************	f Summary							
Subbasin ID	Accumulate Preci i	p Inte	nfall nsity in/hr	Total Runoff in	Runoff	Weighted Runoff Coeff	Conc	Time of entration hh:mm:ss
DC-01 DC-02 DC-03 DC-04 DC-05 DC-06	0.4 0.4 0.3 0.3 0.5 0.4	1 5 8 9	1.65 1.82 2.08 1.96 1.25 1.66	0.25 0.24 0.17 0.05 0.13 0.10	6.65 2.20 1.62 0.25 0.72	0.550 0.590 0.500 0.130 0.220	0 0 0 0 0	00:16:52 00:13:40 00:09:59 00:11:32 00:28:07 00:16:36
**************************************	mary							
Node ID	Average Depth Attained	Depth	HGI	. Occi		Total Flooded Volume	Time	
	ft 	ft			hh:mm			hh:mm:ss

SDCI-K3	0.06	1.24	4541.91	0	00:17	0	0	0:00:00
SDCI-K4	0.04	1.31	4542.13	0	00:17	0	0	0:00:00
SDCI-L2	0.00	0.51	4541.76	0	00:10	0	0	0:00:00
SDMH-K2	0.21	1.35	4541.42	0	00:34	0	0	0:00:00
SDMH-N2	0.05	0.14	4530.74	0	01:00	0	0	0:00:00
SDMH-N3	0.04	0.14	4533.45	0	00:52	0	0	0:00:00
SDMH-N4	0.04	0.14	4536.03	0	00:43	0	0	0:00:00
SDMH-N5	0.05	0.15	4537.51	0	00:35	0	0	0:00:00
SDMH-N6-M1	0.05	0.15	4538.91	0	00:27	0	0	0:00:00
SDOS-M5	0.04	0.14	4539.30	0	00:34	0	0	0:00:00
D5	0.00	0.00	0.00	0	00:00	0	0	0:00:00
D6	0.00	0.00	0.00	0	00:00	0	0	0:00:00
SDMH-N1	0.04	0.14	4530.40	0	01:00	0	0	0:00:00
Pond	0.57	2.26	4541.42	0	00:33	0	0	0:00:00

Node ID	Element Type	Maximum Lateral Inflow cfs	Peak Inflow cfs	Peak Occu	ime of Inflow irrence hh:mm	Flooding	Occurrence
SDCI-K3	JUNCTION	2.20	8.32	0	00:17	0.00	
SDCI-K4	JUNCTION	6.65	6.65	0	00:16	0.00	
SDCI-L2	JUNCTION	1.62	1.62	0	00:10	0.00	
SDMH-K2	JUNCTION	0.00	8.27	0	00:17	0.00	
SDMH-N2	JUNCTION	0.00	0.12	0	00:55	0.00	
SDMH-N3	JUNCTION	0.00	0.12	0	00:47	0.00	
SDMH-N4	JUNCTION	0.00	0.12	0	00:40	0.00	
SDMH-N5	JUNCTION	0.00	0.12	0	00:30	0.00	
SDMH-N6-M1	JUNCTION	0.00	0.12	0	00:34	0.00	
SDOS-M5	JUNCTION	0.00	0.12	0	00:33	0.00	
D5	OUTFALL	0.72	0.72	0	00:28	0.00	
D6	OUTFALL	0.26	0.26	0	00:16	0.00	
SDMH-N1	OUTFALL	0.00	0.12	0	01:00	0.00	
Pond	STORAGE	0.25	8.85	0	00:16	0.00	

-	ge Node ID Time of Max.	Maximum Total	Maximum	Time of Max	Average	Average	Maximum
11011111110111	110 01 110111	Ponded	Ponded	Ponded	Ponded	Ponded	Storage Node
Exfiltra	ation Exfiltr	ation Exfiltr	rated				-
		Volume	Volume	Volume	Volume	Volume	Outflow
Rate	Rate	Volume					
		1000 ft³	(%)	days hh:mm	1000 ft³	(%)	cfs
cfm	hh:mm:ss	1000 ft³					
Pond		9.036	10	0 00:33	1.492	2.	0.32
0.00	0:00:00	0.000	10	0 00.33	1.152	2	0.02

Outfall Node ID	Flow	Average	Peak
	Frequency	Flow	Inflow
	(%)	cfs	cfs
D5	0.98	0.36	0.72
D6	0.58	0.13	0.26
SDMH-N1	45.30	0.06	0.12
System	15.62	0.55	0.80

Link Flow Summary ********

Link ID		Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of	Тс	tal Reported	_						
Maximum	Тi	Type .me Condition	Pea	k Flow	Velocity	Factor	during	Flow	Maximum
Haniman		inc conarcion	Occu	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharg	red			1-1	C+ /				7 1
Depth minu	ıt.e.s	3	days	hh:mm	ft/sec		cfs	cfs	Flow
Dopon mino									
K1-K2		CONDUIT	0	00:17	4.44	1.00	8.17	16.00	0.51
0.75	0								
K2-K3 0.63	0	CONDUIT Calculated	0	00:17	4.01	1.00	8.27	16.06	0.51
K3-K4	U	CONDUIT	0	00:17	3.14	1.00	6.64	15.74	0.42
0.64	0	Calculated							
L1-L2 0.33	0	CONDUIT Calculated	0	00:10	3.16	1.00	1.58	7.40	0.21
M1-M2	U	CONDUIT	0	00:34	1.36	1.00	0.12	6.61	0.02
0.10	0	Calculated							
N1-N2 0.09	0	CONDUIT Calculated	0	01:00	1.40	1.00	0.12	6.63	0.02
N2-N3	U	CONDUIT	0	00:55	1.44	1.00	0.12	6.61	0.02
0.09	0	Calculated							
N3-N4 0.09	0	CONDUIT Calculated	0	00:47	1.55	1.00	0.12	6.64	0.02
N4-N5	U	Calculated	0	00:40	1.35	1.00	0.12	5.84	0.02
0.10	0	Calculated							
N5-N6 0.10	0	CONDUIT Calculated	0	00:30	1.30	1.00	0.12	5.85	0.02
Pond-Outlet	U	OUTLET	0	00:33			0.12		
			-						

******** All links are stable.

Analysis began on: Thu Mar 2 19:51:12 2023 Analysis ended on: Thu Mar 2 19:51:23 2023 Total elapsed time: 00:00:11

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.4.133 (Build 0)
******
Project Description
File Name ...... 2060-001 PR Model - Rational 100-YR.SPF
*****
Analysis Options
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... User-Defined
Return Period...... 100 years
Link Routing Method ..... Hydrodynamic
Storage Node Exfiltration.. Horton, wetted area
Starting Date ..... JUL-04-2017 00:00:00
Ending Date ..... JUL-08-2017 00:00:00
Report Time Step ..... 00:00:10
*****
Element Count
Number of subbasins ..... 6
Number of nodes ..... 14
Number of links ..... 11
Subbasin Summary
Subbasin
                Total
             7.35
2.05
DC-01
DC-02
DC-03
                 1.56
DC-04
                 0.98
                 2.62
DC-05
DC-06
                 0.75
*****
Node Summary
             Node
            Type
______
```

Pond	STO	ORAGE	4539.	16 4546.4	0.00		
************* Link Summary ********* Link ID	У	ode	To Node	Element Type	Lengtl ft	-	Manning's Roughness
K1-K2 K2-K3 K3-K4 L1-L2 M1-M2 N1-N2 N2-N3 N3-N4 N4-N5 N5-N6 Pond-Outlet	SDMH-K2 SDCI-K3 SDCI-K4 SDCI-L2 SDOS-M5 SDMH-N2 SDMH-N3 SDMH-N4 SDMH-N5 SDMH-N6 Pond	3 4 2 5 5 2 3 3 4 5	Pond SDMH-K2 SDCI-K3 Pond SDMH-N6-M1 SDMH-N1 SDMH-N2 SDMH-N3 SDMH-N4 SDMH-N5 SDOS-M5	CONDUIT	119.0 31.0 115.0 101.0 85.3 685.0 645.0	0.5042 0.4839 0.4957 0.3960 0.3986 0.3956 0.4000 0.3095	0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130
**************************************	on Summary						
Link Design	Shape		Depth/	Width	No. of	Cross	Full Flow
ID Flow			Diameter		Barrels	Sectional	Hydraulic
Capacity			5.	5.		Area	Radius
cfs			ft	ft		ft²	ft
K1-K2 16.00	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
K2-K3 16.06	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
K3-K4 15.74	CIRCUI	LAR	2.00	2.00	1	3.14	0.50
L1-L2 7.40	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
M1-M2 6.61	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
N1-N2	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.63 N2-N3	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.61 N3-N4	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
6.64 N4-N5	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
5.84 N5-N6 5.85	CIRCUI	LAR	1.50	1.50	1	1.77	0.38
************* Transect Sur ********	mmary ****						
Transect C&0 Area:		0 0007	0.0015	0 0007	0.0040		
	0.0002 0.0060 0.0323	0.0007 0.0087 0.0414	0.0015 0.0126 0.0519	0.0027 0.0179 0.0637	0.0042 0.0244 0.0767		

Soil/Surf	ace Descript	tion			Area (acres)	Soil Group	Runoff Coeff.
Subbasin :							
_	Area & Weig	ghted Runof	f Coeff.		5.21 5.21	-	0.71 0.71
Soil/Surfa	ace Descript	tion			Area (acres)	Soil Group	Runoff Coeff.
Subbasin	DC-01						
Runoff Co	********** efficient Co *****	omputations	Report				
	y Error (%)		0.000	21230			
Initial S	Outflow tored Volume red Volume	e	0.641 0.000 0.000	0.209 0.000 0.000			
External	Inflow		0.000	0.000			
Flow Rout	************* ing Continu: ******	ity	Volume acre-ft	Volume Mgallons			
	cipitation y Error (%)		1.001 0.359	0.784			
Runoff Qu	*********** antity Cont	inuity	Volume acre-ft	Depth inches			
	1.0000	1.0000	1.0000	1.0000	1.0000		
	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000	1.0000 1.0000 1.0000		
	0.5415 1.0000	0.6133 1.0000	0.7100 1.0000	0.8067 1.0000	0.9033 1.0000		
	0.0121 0.0723 0.3069	0.0241 0.1193 0.3539	0.0362 0.1662 0.4008	0.0482 0.2131 0.4477	0.0603 0.2600 0.4946		
Width:	0.8958	0.9220	0.9481	0.9741	1.0000		
	0.3506 0.4909 0.6284 0.7634	0.3789 0.5186 0.6556 0.7901	0.4070 0.5462 0.6827 0.8167	0.4351 0.5737 0.7097 0.8432	0.4630 0.6011 0.7366 0.8696		
	0.1760 0.2076	0.1828 0.2364	0.1855 0.2651	0.1911 0.2937	0.1986 0.3222		
Hrad:	0.0139 0.0834 0.1095	0.0278 0.0743 0.1222	0.0417 0.0783 0.1352	0.0556 0.0869 0.1486	0.0695 0.0976 0.1622		
	0.7506 0.8891	0.7783 0.9169	0.8060 0.9446	0.8337 0.9723	0.8614		
	0.3349 0.4735 0.6120	0.3626 0.5012 0.6397	0.3903 0.5289 0.6674	0.4180 0.5566 0.6952	0.4457 0.5843 0.7229		
	0.0911 0.1963	0.1069 0.2240	0.1252 0.2518	0.1463 0.2795	0.1700 0.3072		

- Composite Area	& Weighted	Runoff C	oeff.			2.05 2.05	-	0.73 0.73
Subbasin DC-03								
Soil/Surface De	escription					rea res)	Soil Group	Runoff Coeff.
- Composite Area	& Weighted	Runoff C	coeff.			1.56 1.56	-	0.68
Subbasin DC-04								
Soil/Surface De						rea res)	Soil Group	
- Composite Area		Runoff C	oeff.			0.98 0.98	-	0.47 0.47
Subbasin DC-05								
Soil/Surface De	escription					rea res)	Soil Group	Runoff Coeff.
- Composite Area	& Weighted	Runoff C	coeff.			2.62 2.62	_	0.52 0.52
Subbasin DC-06								
Soil/Surface De	escription					rea res) 	Soil Group	Runoff Coeff.
- Composite Area	& Weighted	Runoff C	coeff.			0.75 0.75	-	0.52 0.52
**************************************	f Summary							
Subbasin ID	Accumulate Preci	p Inte	nfall nsity in/hr	Total Runoff in	Runoff	Weighted Runoff Coeff	Conc	Time of entration hh:mm:ss
DC-01 DC-02 DC-03 DC-04 DC-05 DC-06	0.7 0.7 0.5 0.6 1.0	1 9 4 0	2.81 3.10 3.55 3.34 2.13 2.83	0.56 0.52 0.40 0.30 0.52 0.41	14.66 4.64 3.76 1.54 2.91	0.710 0.730 0.680 0.470 0.520	0 0 0 0	00:16:52 00:13:40 00:09:59 00:11:32 00:28:07 00:16:36
**************************************	nary							
Node ID	Average Depth Attained	Depth	HGI	. Occi		Total Flooded Volume	Time	
	ft	ft 			hh:mm			hh:mm:ss

SDCI-K3	0.18	3.42	4544.09	0	00:17	0	0	0:00:00
SDCI-K4	0.14	3.73	4544.55	0	00:17	0.00	4	0:00:00
SDCI-L2	0.06	1.44	4542.69	0	00:31	0	0	0:00:00
SDMH-K2	0.38	2.72	4542.79	0	00:19	0	0	0:00:00
SDMH-N2	0.07	0.69	4531.29	0	00:41	0	0	0:00:00
SDMH-N3	0.07	0.62	4533.93	0	00:37	0	0	0:00:00
SDMH-N4	0.07	0.63	4536.52	0	00:34	0	0	0:00:00
SDMH-N5	0.07	0.70	4538.06	0	00:31	0	0	0:00:00
SDMH-N6-M1	0.07	0.68	4539.44	0	00:26	0	0	0:00:00
SDOS-M5	0.07	0.70	4539.86	0	00:31	0	0	0:00:00
D5	0.00	0.00	0.00	0	00:00	0	0	0:00:00
D6	0.00	0.00	0.00	0	00:00	0	0	0:00:00
SDMH-N1	0.07	0.61	4530.87	0	00:41	0	0	0:00:00
Pond	0.84	3.50	4542.66	0	00:31	0	0	0:00:00

Node ID	Element Type	Maximum Lateral Inflow cfs	Peak Inflow cfs	Peak Occu	ime of Inflow rrence hh:mm	Flooding	Fl Occu	f Peak ooding rrence hh:mm
SDCI-K3	JUNCTION	4.64	18.13	0	00:17	0.00		
SDCI-K4	JUNCTION	14.66	14.66	0	00:17	0.17	0	00:16
SDCI-L2	JUNCTION	3.76	3.76	0	00:10	0.00		
SDMH-K2	JUNCTION	0.00	18.13	0	00:17	0.00		
SDMH-N2	JUNCTION	0.00	2.33	0	00:38	0.00		
SDMH-N3	JUNCTION	0.00	2.32	0	00:35	0.00		
SDMH-N4	JUNCTION	0.00	2.31	0	00:32	0.00		
SDMH-N5	JUNCTION	0.00	2.31	0	00:28	0.00		
SDMH-N6-M1	JUNCTION	0.00	2.28	0	00:31	0.00		
SDOS-M5	JUNCTION	0.00	2.28	0	00:31	0.00		
D5	OUTFALL	2.91	2.91	0	00:28	0.00		
D6	OUTFALL	1.10	1.10	0	00:16	0.00		
SDMH-N1	OUTFALL	0.00	2.29	0	00:41	0.00		
Pond	STORAGE	1.54	20.35	0	00:14	0.00		

	ge Node ID Time of Max.	Maximum Total	Maximum	Time of Max	Average	Average	Maximum
		Ponded	Ponded	Ponded	Ponded	Ponded	Storage Node
Exfiltra	ation Exfiltr	ation Exfilt	rated				-
		Volume	Volume	Volume	Volume	Volume	Outflow
Rate	Rate	Volume					
		1000 ft ³	(%)	days hh:mm	1000 ft³	(%)	cfs
cfm	hh:mm:ss	1000 ft³					
Pond 0.00	0:00:00	19.203 0.000	21	0 00:31	2.712	3	2.55

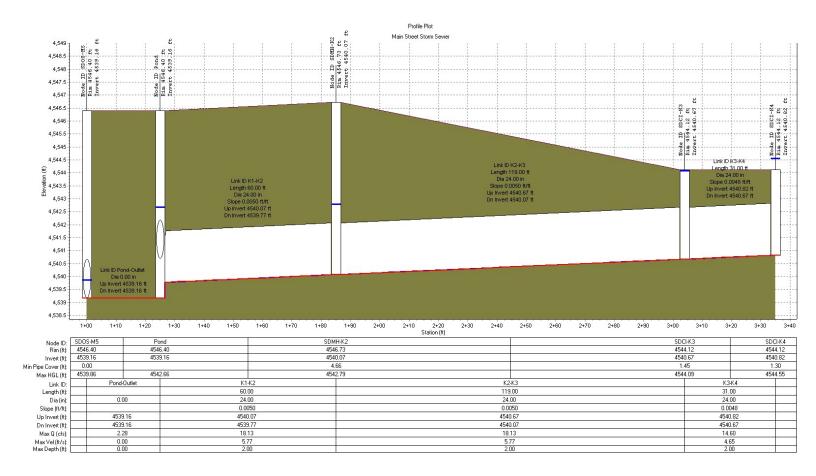
Outfall Node ID	Flow	Average	Peak
	Frequency	Flow	Inflow
	(%)	cfs	cfs
D5	0.98	1.46	2.91
D6	0.58	0.55	1.10
SDMH-N1	55.40	0.11	2.29
System	18.99	2.13	4.08

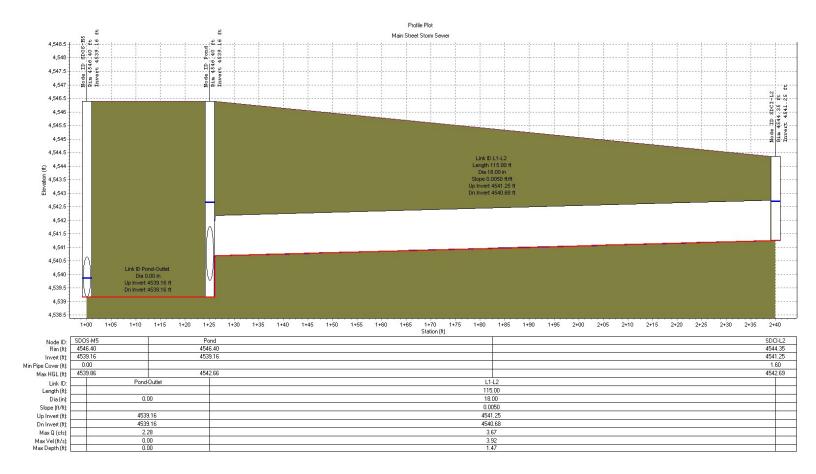
Link Flow Summary ********

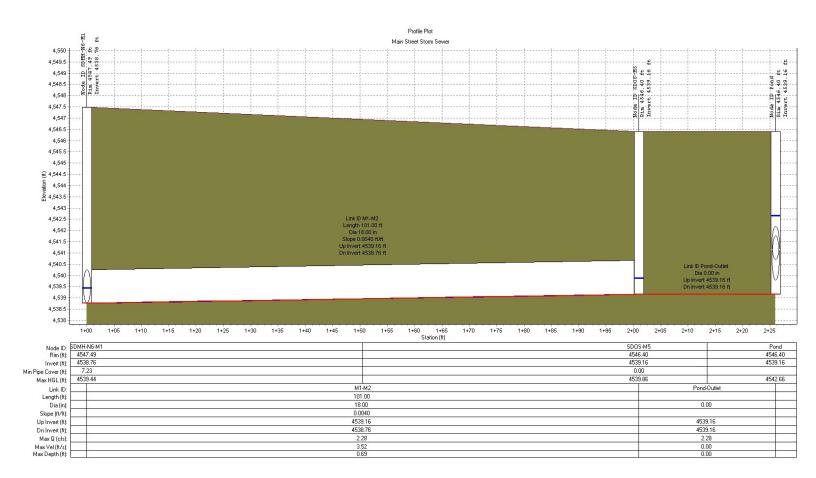
Link ID		Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of	То	tal Reported	_	:	7				
Maximum	Тi	Type me Condition	Pea	K F.TOM	Velocity	Factor	during	Flow	Maximum
11011111111111		001101011	Occu	rrence	Attained		Analysis	Capacity	/Design
Flow Surchard	ged		.1	1. 1	C+ /			- 6 -	7 1
Depth minu	ıtes		days	hh:mm	ft/sec		cfs	cfs	Flow
верен шти	2000								
K1-K2		CONDUIT	0	00:17	5.77	1.00	18.13	16.00	1.13
	117	SURCHARGED							
K2-K3 1.00	1.0	CONDUIT	0	00:17	5.77	1.00	18.13	16.06	1.13
K3-K4	18	SURCHARGED CONDUIT	0	00:17	4.65	1.00	14.60	15.74	0.93
1.00	16	SURCHARGED	ŭ	00.1	1.00	1.00	11.00	10.71	0.30
L1-L2	0	CONDUIT	0	00:10	3.92	1.00	3.67	7.40	0.50
0.98 M1-M2	0	Calculated CONDUIT	0	00:31	3.52	1.00	2.28	6.61	0.35
0.46	0	Calculated	O	00.51	3.32	1.00	2.20	0.01	0.33
N1-N2		CONDUIT	0	00:41	3.14	1.00	2.29	6.63	0.35
0.43 N2-N3	0	Calculated CONDUIT	0	00:38	3.30	1.00	2.33	6.61	0.35
0.43	0	Calculated	0	00.50	3.30	1.00	2.33	0.01	0.55
N3-N4		CONDUIT	0	00:35	3.66	1.00	2.32	6.64	0.35
0.41 N4-N5	0	Calculated CONDUIT	0	00:32	3.37	1.00	2.31	5.84	0.39
0.44	0	Calculated	U	00:32	3.37	1.00	2.31	3.04	0.39
N5-N6	-	CONDUIT	0	00:28	3.47	1.00	2.31	5.85	0.40
0.45	0	Calculated	0	00 21			2 22		
Pond-Outlet		OUTLET	0	00:31			2.28		

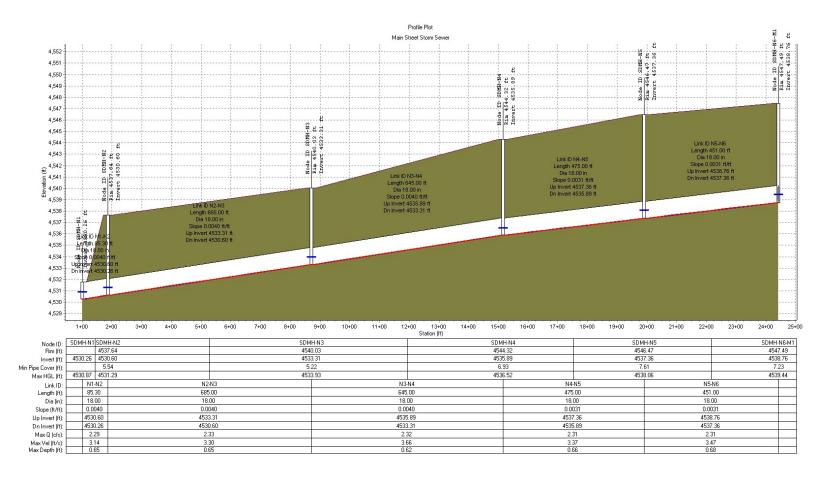
Link Pond-Outlet (2)

Analysis began on: Thu Mar 2 19:33:01 2023 Analysis ended on: Thu Mar 2 19:33:13 2023 Total elapsed time: 00:00:12









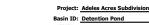
APPENDIX D

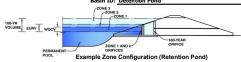
Proposed Detention Pond

- 1. Mile High Flood District Detention Basin Design Workbook
 - a. Design Information & Stage Storage
 - b. Outlet Structure Design
 - c. Hydrograph, Drain Time, and Ponding Depth Graphs

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.05 (January 2022)





Watershed Information

Selected BMP Type =	EDB						
Watershed Area =	11.93	acres					
Watershed Length =	910	ft					
Watershed Length to Centroid =	455	ft					
Watershed Slope =	0.005	ft/ft					
Watershed Imperviousness =	56.40%	percent					
Percentage Hydrologic Soil Group A =	0.0%	percent					
Percentage Hydrologic Soil Group B =	100.0%	percent					
Percentage Hydrologic Soil Groups C/D =	0.0%	percent					
Target WQCV Drain Time =	40.0	hours					
Location for 1-hr Rainfall Depths = User Input							

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

the embedded Colorado Urban Hydro	grapn Procedu	re.
Water Quality Capture Volume (WQCV) =	0.223	acre-fee
Excess Urban Runoff Volume (EURV) =	0.726	acre-fee
2-yr Runoff Volume (P1 = 0.47 in.) =	0.204	acre-fee
5-yr Runoff Volume (P1 = 0.63 in.) =	0.290	acre-fee
10-yr Runoff Volume (P1 = 0.77 in.) =	0.368	acre-fee
25-yr Runoff Volume (P1 = 0.97 in.) =	0.512	acre-fee
50-yr Runoff Volume (P1 = 1.13 in.) =	0.644	acre-fee
100-yr Runoff Volume (P1 = 1.31 in.) =	0.830	acre-fee
500-yr Runoff Volume (P1 = 1.74 in.) =	1.254	acre-fee
Approximate 2-yr Detention Volume =	0.218	acre-fee
Approximate 5-yr Detention Volume =	0.315	acre-fee
Approximate 10-yr Detention Volume =	0.429	acre-fee
Approximate 25-yr Detention Volume =	0.515	acre-fee
Approximate 50-yr Detention Volume =	0.557	acre-fee
Approximate 100-yr Detention Volume =	0.634	acre-fee

Optional User Overrides

acre-feet
acre-feet
inches

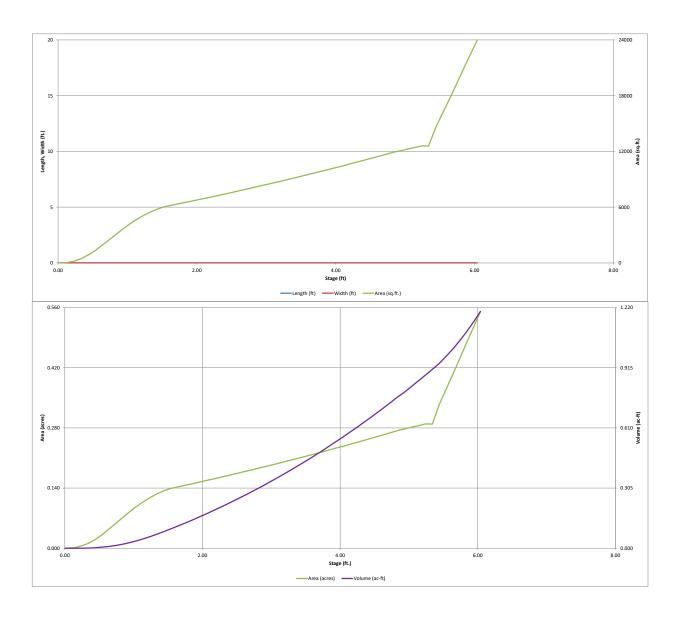
Define Zones and Basin Geometry

reme Lones and Basin Geometry		
Zone 1 Volume (WQCV) =	0.223	acre-feet
Zone 2 Volume (10-year - Zone 1) =	0.206	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.205	acre-feet
Total Detention Basin Volume =	0.634	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth (H _{total}) =	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S_{TC}) =	user	ft/ft
Slopes of Main Basin Sides (Smain) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	
		•

Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length (L _{ISV}) =	user	ft
Surcharge Volume Width (W _{ISV}) =	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor (W _{FLOOR}) =	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W _{MAIN}) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Basin Volume (Vtotal) =	user	acre-fe

		1							
Depth Increment =	0.10	ft Optional			I	Optional			
Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
Top of Micropool	(ft)	Stage (ft) 0.00	(ft)	(ft)	(ft²)	Area (ft ²)	(acre) 0.000	(ft 3)	(ac-ft)
Top of Pileropoor		0.04		-	-	4	0.000	0	0.000
	-	0.14	-	-		58	0.001	3	0.000
	-	0.24	-	-		217	0.005	17	0.000
	-	0.34				489	0.011	52	0.001
	-	0.44		-		871	0.020	120	0.003
		0.54		-		1,358	0.031	232 396	0.005
	-	0.74		-		2,506	0.058	617	0.009
	-	0.84				3,098	0.071	897	0.021
	-	0.94				3,689	0.085	1,237	0.028
		1.04		-		4,235	0.097	1,633	0.037
		1.14				4,721	0.108	2,081	0.048
		1.24		-	-	5,146 5,512	0.118 0.127	2,574 3,107	0.059
		1.44	-			5,817	0.134	3,673	0.084
		1.54	-			6,059	0.139	4,267	0.098
		1.64				6,218	0.143	4,881	0.112
	-	1.74				6,370	0.146	5,510	0.126
		1.84		-		6,523 6,679	0.150 0.153	6,155 6,815	0.141 0.156
	-	2.04			-	6,836	0.157	7,491	0.172
		2.14		-		6,995	0.161	8,182	0.188
		2.24		-		7,155	0.164	8,890	0.204
	-	2.34		-	-	7,318	0.168	9,613	0.221
	-	2.44				7,482 7,647	0.172	10,353	0.238 0.255
	-	2.54				7,647	0.176 0.179	11,110	0.255
	-	2.74				7,984	0.183	12,673	0.291
		2.84				8,155	0.187	13,480	0.309
		2.94		-	-	8,327	0.191	14,304	0.328
		3.04		-		8,501	0.195 0.199	15,145	0.348
	_	3.14 3.24		-		8,677 8,855	0.199	16,004 16,881	0.367
		3.34				9,034	0.207	17,775	0.408
	-	3.44		-		9,215	0.212	18,688	0.429
		3.54		-		9,397	0.216	19,618	0.450
		3.64				9,582	0.220	20,567	0.472
		3.74		-	-	9,768 9,956	0.224	21,535 22,521	0.494 0.517
		3.94		-	-	10,145	0.233	23,526	0.540
		4.04			-	10,336	0.237	24,550	0.564
		4.14		-	-	10,529	0.242	25,593	0.588
		4.24		-		10,724	0.246	26,656	0.612
		4.34 4.44		-	-	10,920 11,118	0.251 0.255	27,738 28,840	0.637
		4.54			_	11,318	0.260	29,962	0.688
		4.64		-	-	11,519	0.264	31,104	0.714
		4.74			-	11,722	0.269	32,266	0.741
		4.84				11,927	0.274	33,448	0.768
		4.94 5.04		-		12,098 12,266	0.278 0.282	34,528 35,745	0.793 0.821
		5.14		-	-	12,431	0.285	36,978	0.849
		5.24		-	-	12,592	0.289	38,228	0.878
		5.34		-	-	12,589	0.289	39,487	0.906
		5.44		-		14,559	0.334	40,825	0.937
		5.54 5.64		-		16,104 17,665	0.370 0.406	42,343 44,016	0.972 1.010
		5.74		-	-	19,240	0.442	45,845	1.052
		5.84		-	-	20,859	0.479	47,834	1.098
		5.94		-	-	22,419	0.515	49,982	1.147
		6.04		-		23,984	0.551	52,287	1.200
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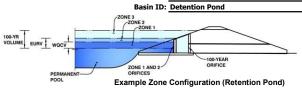


2060-001 MHFD-Detention_v4-05.xism, Basin 3/2/2023, 7:39 PM

DETENTION BASIN OUTLET STRUCTURE DESIGN

MHFD-Detention, Version 4.05 (January 2022)

Project: Adeles Acres Subdivision



	Estimated	Estimated	
	Stage (ft)	Volume (ac-ft)	Outlet Type
Zone 1 (WQCV)	2.36	0.223	Orifice Plate
Zone 2 (10-year)	3.45	0.206	Rectangular Orifice
one 3 (100-year)	4.33	0.205	Weir&Pipe (Restrict)
	Total (all zones)	0.634	

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) N/A Underdrain Orifice Diameter = N/A inches

	Calculated Parame	ters for Underdrain
Underdrain Orifice Area =	N/A	ft ²
Underdrain Orifice Centroid =	N/A	feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BI

Centroid of Lowest Orifice =	0.00	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate =	2.36	ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing =	9.40	inches
Orifice Plate: Orifice Area per Row =	0.99	sq. inches (diameter = 1-1/8 inches)

BMP)	Calculated Parame	ters for Plate
WQ Orifice Area per Row =	6.875E-03	ft ²
Elliptical Half-Width =	N/A	feet
Elliptical Slot Centroid =	N/A	feet
Elliptical Slot Area =	N/A	ft ²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.79	1.57					
Orifice Area (sq. inches)	0.99	0.99	0.99					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Zone 2 Rectangular	Not Selected		
Invert of Vertical Orifice =	2.36	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Area
Depth at top of Zone using Vertical Orifice =	3.45	N/A	ft (relative to basin bottom at Stage = 0 ft)	Vertical Orifice Centroid
Vertical Orifice Height =	2.50	N/A	inches	
Vertical Orifice Width =	3.00		inches	

	Calculated Parameters for Vertical Orifice					
	Zone 2 Rectangular	Not Selected				
e Area =	0.05	N/A	ft ²			
entroid =	0.10	N/A	feet			

User Input: Overflow Weir	Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir and No Outlet Pipe)

nput: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/ Trapezoidal Weir and No Outlet Pipe)					Calculated Parameters for Overflow Weir		
	Zone 3 Weir	Not Selected		Zone 3 Weir	Not Selected	1	
Overflow Weir Front Edge Height, Ho =	3.05	N/A	ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t =	3.05	N/A	feet	
Overflow Weir Front Edge Length =	2.92	N/A	feet Overflow Weir Slope Length =	2.92	N/A	feet	
Overflow Weir Grate Slope =	0.00	N/A	H:V Grate Open Area / 100-yr Orifice Area =	22.79	N/A		
Horiz. Length of Weir Sides =	2.92	N/A	feet Overflow Grate Open Area w/o Debris =	5.93	N/A	ft ²	
Overflow Grate Type =	Type C Grate	N/A	Overflow Grate Open Area w/ Debris =	5.93	N/A	ft ²	
Debris Cloaging % =	0%	N/A	 %				

<u>User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate</u>, or Rectangular Orifice)

er Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)				Calculated Parameters	s for Outlet Pipe w/	Flow Restriction P	late_
	Zone 3 Restrictor	Not Selected			Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.00	N/A	ft (distance below basin bottom at Stage = 0 ft)	Outlet Orifice Area =	0.26	N/A	ft ²
Outlet Pipe Diameter =	18.00	N/A	inches	Outlet Orifice Centroid =	0.18	N/A	feet
Restrictor Plate Height Above Pipe Invert =	3.69	•	inches Half-Central Angle of	Restrictor Plate on Pipe =	0.94	N/A	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

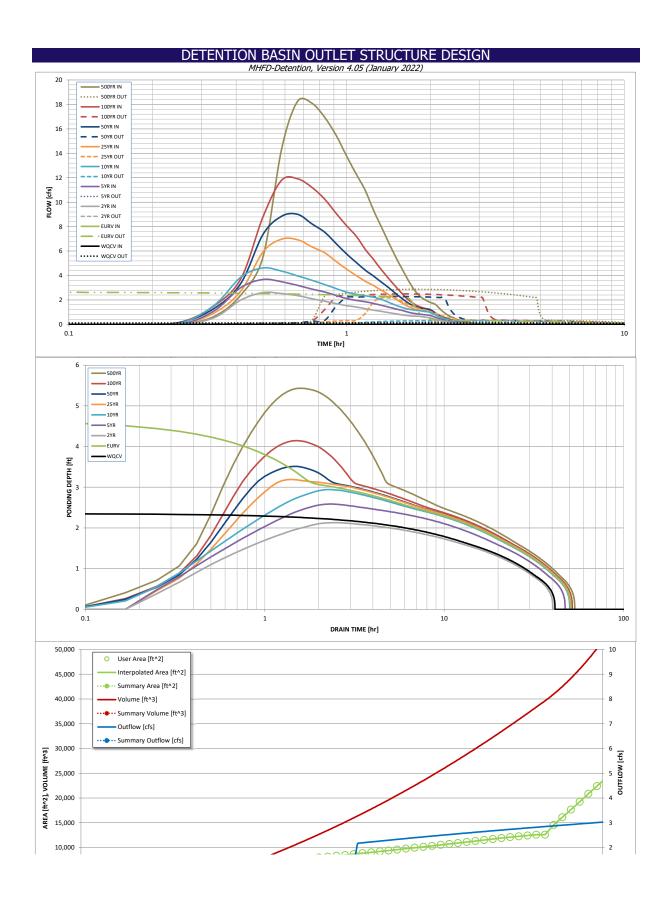
Spillway Invert Stage=	ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length =	feet
Spillway End Slopes =	H:V
Freeboard above Max Water Surface =	feet

Calculated	Parameters	for	Spillway

Spillway Design Flow Depth=	feet
Stage at Top of Freeboard =	feet
Basin Area at Top of Freeboard =	acres
Basin Volume at Top of Freeboard =	acre-ft

Rout

outed Hydrograph Results	The user can override the default CUHP hydrographs and runoff volumes by entering new values in the Inflow Hydrographs table (Columns W through AF).								
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	0.47	0.63	0.77	0.97	1.13	1.31	1.74
Structure Controlling Flow =	Vertical Orifice 1	Outlet Plate 1	Plate	Vertical Orifice 1	Vertical Orifice 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	0.35	N/A	N/A	N/A	0.3	0.3	0.3	0.4
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	41	37	43	44	43	42	41	39
Time to Drain 99% of Inflow Volume (hours) =	40	47	39	45	48	48	48	47	47
•									



DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

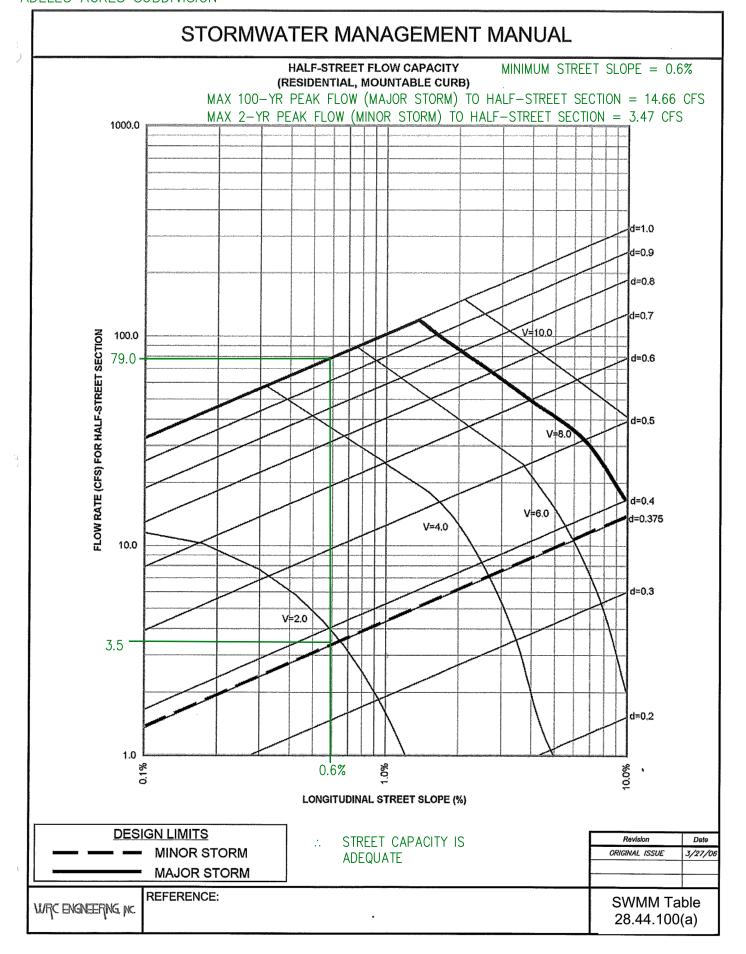
The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:15:00	0.00	0.00	0.00	0.00	0.08	0.00	0.14	0.17	0.65
	0:20:00	0.00	0.00	0.54	1.11	1.56	0.94	1.30	1.52	2.42
}	0:25:00	0.00	0.00	2.00	3.03 3.67	3.88 4.61	2.74 5.92	3.38 7.37	3.76 8.80	5.53 14.34
ŀ	0:35:00	0.00	0.00	2.53	3.49	4.36	6.97	8.84	11.80	18.28
	0:40:00	0.00	0.00	2.35	3.18	3.97	6.92	9.00	11.91	18.11
	0:45:00	0.00	0.00	2.10	2.89	3.61	6.35	8.23	11.22	16.95
	0:50:00	0.00	0.00	1.89	2.65	3.26	5.86	7.55	10.25	15.47
	0:55:00	0.00	0.00	1.70	2.37	2.93	5.16	6.61	9.09	13.78
	1:00:00	0.00	0.00	1.53	2.12	2.64	4.52	5.76	8.08	12.29
ŀ	1:05:00	0.00	0.00	1.42	1.96	2.46	4.00	5.07	7.22	10.98
ŀ	1:15:00	0.00	0.00	1.29 1.17	1.85 1.72	2.34	3.54 3.18	4.44 3.95	6.15 5.31	9.34 8.00
	1:20:00	0.00	0.00	1.06	1.56	2.05	2.80	3.46	4.48	6.70
	1:25:00	0.00	0.00	0.96	1.41	1.81	2.45	3.01	3.75	5.55
	1:30:00	0.00	0.00	0.87	1.27	1.58	2.08	2.54	3.11	4.54
	1:35:00	0.00	0.00	0.78	1.14	1.39	1.75	2.11	2.52	3.62
	1:40:00	0.00	0.00	0.71	1.00	1.25	1.46	1.75	2.02	2.84
	1:45:00	0.00	0.00	0.68	0.90	1.17	1.27	1.50	1.67	2.33
	1:55:00	0.00	0.00	0.66	0.84	1.12	1.15	1.35	1.45	2.01
	2:00:00	0.00	0.00	0.59 0.53	0.79 0.73	1.06 0.98	1.07 1.02	1.25 1.19	1.31 1.22	1.80 1.65
	2:05:00	0.00	0.00	0.42	0.58	0.78	0.81	0.94	0.95	1.03
	2:10:00	0.00	0.00	0.33	0.45	0.60	0.62	0.72	0.71	0.95
	2:15:00	0.00	0.00	0.25	0.35	0.47	0.48	0.56	0.54	0.71
	2:20:00	0.00	0.00	0.19	0.27	0.36	0.37	0.42	0.41	0.54
	2:25:00	0.00	0.00	0.15	0.20	0.27	0.28	0.32	0.31	0.41
ŀ	2:30:00	0.00	0.00	0.11	0.15	0.20	0.21	0.24	0.23	0.31
	2:35:00	0.00	0.00	0.08	0.11	0.15 0.11	0.15 0.12	0.18	0.17 0.13	0.23 0.17
	2:45:00	0.00	0.00	0.00	0.06	0.08	0.12	0.13	0.13	0.17
	2:50:00	0.00	0.00	0.03	0.04	0.06	0.06	0.07	0.07	0.09
	2:55:00	0.00	0.00	0.02	0.03	0.04	0.04	0.04	0.04	0.05
	3:00:00	0.00	0.00	0.01	0.01	0.02	0.02	0.02	0.02	0.03
	3:05:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
ŀ	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00 3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
[3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
}	3:50:00 3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00 4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
}	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
l	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

APPENDIX E

Street and Inlet Capacity Checks & Riprap Sizing

- 1. Half-Street Flow Capacity SWMM Table 28.44.100(a)
- 2. Sump Inlet Capacity SWMM Table 28.44.130
- 3. SWMM Table 28.32.200 & Riprap Calculations



STORMWATER MANAGEMENT MANUAL

Maximum Inlet Capacities Sump or Sag Condition

			(3-INCH VER	TICAL CUR	В	
	INLET TYPE	SIN	GLE	DOUBLE		TRI	PLE
***************************************		2-YR	100-YR	2-YR	100-YR	2-YR	100-YR
RB- G ION	COMBINATION INLET (TYPE D GRATES)	9.8	12.4	14.7	20.1	19.6	27.8
2-INCH CURB. OPENING DEPRESSION	COMBINATION INLET (TYPE R GRATES)	9.8	11.1	14.7	18.8	19.6	26.5
2-IN O DEI	CURB-OPENING INLET CAPACITY	7.7	10.3	12.7	20.6	15.0	30.9
ENING	COMBINATION INLET (TYPE D GRATES)	6.4	9.3	9.5	14.2	12.7	19.1
CURB-OPENING DEPRESSION	COMBINATION INLET (TYPE R GRATES)	5.1	8.1	9.5	13.0	12.7	17.9
NO CL DEI	CURB-OPENING INLET CAPACITY	4.1	6.5	8.3	13.1	12.4	19.6

SDCI-L2 IS A SINGLE CURB INLET, SDCI-K3 & SDCI-K4 ARE DOUBLE CURB INLETS

			4.5-INCH MOUNTABLE CURB					
		INLET TYPE	SINGLE		DOUBLE		TRI	PLE
_			2-YR	100-YR	2-YR	100-YR	2-YR	100-YR
	CURB- VING SSION	COMBINATION INLET (TYPE D GRATES)	7.2	10.8	10.8	16.8	14.4	22.7
	2-INCH CURB OPENING DEPRESSION	COMBINATION INLET (TYPE R GRATES)	7.2	9.4	10.8	15.4	14.4	21.4
	2-IN 0 DEI	CURB-OPENING INLET CAPACITY	5.6	8.0	9.3	16.0	11.0	23.9
	ENING	COMBINATION INLET (TYPE D GRATES)	4.1	7.8	6.2	10.9	8.3	14.1
	CURB-OPENING DEPRESSION	COMBINATION INLET (TYPE R GRATES)	. 4.1	6.5	6.2	9.7	8.3	12.8
	NO CL DEI	CURB-OPENING INLET CAPACITY	2.3	4.2	4.7	8.5	7.0	12.7

MAX 2-YR PEAK FLOW TO SINGLE CURB INLET IN SUMP = 0.81 CFS MAX 100-YR PEAK FLOW TO SINGLE CURB INLET IN SUMP = 3.71 CFS See Chart Legend (Figure 1113) for standard inlet lengths.

MAX 2-YR PEAK FLOW TO DOUBLE CURB INLET IN SUMP = 3.47 CFS MAX 100-YR PEAK FLOW TO DOUBLE CURB INLET IN SUMP = 14.66 CFS

Inlet capacities shown above are based upon the following:

- 1. Type D grate used for calculation is Neenah model R-3577.
- 2. Type R grate used for calculation is Neenah model R-3289-C.
- 3. Angled- and curved-vane grates are not allowed for sump or sag design conditions.
- 4. Capacities shown are based upon maximum ponding depths for the 2-year and 100-year storm events:
 - a. 2-year event maximum ponding depth: curb height
 - b. 100-year event maximum ponding depth: 1.0 foot
- 5. Combination inlets are preferred for sump or sag conditions. Curb-opening inlets without grates are allowed.
- 6. Grate-only inlets are not allowed for sump or sag conditions.

INLET	CAPACITIES	ARE
ADEQU	JATE	

Revision	Date
ORIGINAL ISSUE	3/27/06
REVISED CALCULATIONS	12/20/07

WITC ENGNEEPING INC

REFERENCE:

HEC-12, FHWA
WATER-RESOURCES ENGINEERING, LINSLEY (1992)
GRAND JUNCTION STANDARD DETAILS

SWMM Table 28.44.130

STORMWATER MANAGEMENT MANUAL

MAXIMUM PERMISSIBLE MEAN CHANNEL VELOCITY

MATERIAL / LINING

MAXIMUM PERMISSIBLE MEAN VELOCITY (FPS)

NATURAL AND IMPROVED UNLINED CHANNELS

Erosive Soils:

Loams, Sands, Noncolloidal Silts	3.0
Less Erosive Soils:	
Clays, Shales, Cobbles, Gravel	5.0
FULLY-LINED CHANNELS	
Unreinforced Vegetation	5.5
Loose Riprap	
Angular Rock	15.0
Semi-Angular Rock	12.0
Rounded Rock	See Note #4
Grouted Riprap	15.0
Gabions	15.0
Soil Cement	15.0
Concrete	20.0

NOTES:

- 1. For composite lined channels, us the lowest of the maximum mean velocities for the materials used in the composite lining.
- 2. Deviations from the above values are only allowed with appropriate engineering analysis and/or suitable agreements for maintenance responsibilities.
- 3. Maximum permissible velocities based upon non-clear water conditions.
- 4. Suitability of rounded rock as loose riprap material shall be determined by rock particle resistance to movement as a result of shear forces as calculated with a factor of safety of 1.5.

MAX DISCHARGE VELOCITY FROM PIPES:

Pipe K1-K2 = 5.77 FT/S :: RIPRAP IS REQUIRED Pipe L1-L2 = 3.92 FT/S :: RIPRAP IS REQUIRED

Revision	Date
ORIGINAL ISSUE	3/27/06
	¹ Cooper
J 1110 222	

		UNIGHVAL 1330E	3/2//00
WRC ENGNEERING, INC	REFERENCE: NATURAL-MODIFIED FROM FORTIER AND SCOBEY, 1926 FULLY LINED-VARIOUS RESOURCES	SWMM Ta 28.32.20	

Adeles Acres Subdivision

FES SDFE-K1 Outfall to Detention Pond RIP-RAP OUTLET PROTECTION SIZING

REQUIRED INFORMATION:

V =	5.77	ft/sec	Velocity (See Table 805 in the SWMM to verify rip-rap is required)
Q =	18.13	ft ³ /sec	Pipe Discharge
$D_o =$	2.00	ft	Maximum Inside Culvert Width
TW =	2.00	ft	Tailwater Depth (Use normal depth in pipe if unknown)

*See Figure 1209 of the SWMM for a Rip-Rap Mat Diagram

 $D_{50} = (0.02 * Q^{4/3}) / (TW * D_0)$

 D_{50} = Median rock size (ft)

 $D_{50} =$

0.24 ft

2.9 inches

(Use minimum of 6 inch rock)

If TW $< D_o/2$:

DETERMINE REQUIRED APRON LENGTH, La:

$$L_a = [(1.8 * Q) / (D_o^{3/2})] + 7D_o$$

 $L_a = 25.54$

DETERMINE REQUIRED APRON TOP WIDTH, W_T:

 $W_T = 3.0*D_0$

 $W_T = 6.00$

DETERMINE REQUIRED APRON BOTTOM WIDTH, WB:

$$W_B = 3.0*D_o + L_a$$

 $W_B = 31.54$

6 inches L_a = 33.75 feet $W_T =$ 6 feet $W_B =$ 19.5 feet

If TW $\geq D_0/2$:

DETERMINE REQUIRED APRON LENGTH, La:

$$L_a = [(3.0 * Q) / (D_o^{3/2})] + 7D_o$$

 $L_a = 33.23$

430.31 ft² Area= 47.81 yds² 15.94 yds³ (Depth = $2 \times D_{50}$) Volume=

DETERMINE REQUIRED APRON TOP WIDTH, W_T:

 $W_T = 3.0*D_0$

 $W_T = 6.00$

DETERMINE REQUIRED APRON BOTTOM WIDTH, Wa:

 $W_B = 3.0*D_o + 0.4*L_a$

 $W_B = 19.29$

Adeles Acres Subdivision

FES SDFE-L1 Outfall to Detention Pond RIP-RAP OUTLET PROTECTION SIZING

REQUIRED INFORMATION:

***Rirap NOT required at this location, due to low velocity.

V = 3.92 ft/sec Velocity (See Table 805 in the SWMM to verify rip-rap is required)

ft³/sec **Q** = 3.67 Pipe Discharge

D_o = 1.50 ft Maximum Inside Culvert Width TW = 1.47 Tailwater Depth (Use normal depth in pipe if unknown)

*See Figure 1209 of the SWMM for a Rip-Rap Mat Diagram

 $D_{50} = (0.02 * Q^{4/3}) / (TW * D_0)$ D₅₀ = Median rock size (ft)

 $D_{50} =$ **0.05** ft 0.6 inches (Use minimum of 6 inch rock)

If TW $< D_o/2$:

If TW $\geq D_0/2$:

DETERMINE REQUIRED APRON LENGTH, La:

$$L_a = [(1.8 * Q) / (D_o^{3/2})] + 7D_o$$

 $L_a = 14.10$

DETERMINE REQUIRED APRON TOP WIDTH, WT:

 $W_T = 3.0*D_0$

 $W_T = 4.50$

DETERMINE REQUIRED APRON BOTTOM WIDTH, WB:

$$W_B = 3.0*D_o + L_a$$

 $W_B = 18.60$

6 inches $D_{50} =$ L_a = 16.5 feet $W_T =$ 4.5 feet $W_B =$ 11.25 feet

DETERMINE REQUIRED APRON LENGTH, La:

$$L_a = [(3.0 * Q) / (D_o^{3/2})] + 7D_o$$

 $L_a = 16.49$

129.94 ft² Area= 14.44 yds² 4.81 yds³ Volume=

(Depth = $2 \times D_{50}$)

DETERMINE REQUIRED APRON TOP WIDTH, WT:

 $W_T = 3.0*D_0$

 $W_T = 4.50$

DETERMINE REQUIRED APRON BOTTOM WIDTH, Wa:

 $W_B = 3.0*D_o + 0.4*L_a$

 $W_B = 11.10$

APPENDIX F

SWMM Checklists

- 1. Checklist 302
- 2. Checklist 303

Table 302 Stormwater Management Manual Drainage Report Checklist

Instructions: 1.

- Applicant to identify with a "check-mark" if information is provided with report. If applicant believes information is not required, indicate with "n/a" and attach separate sheet with explanation
- 2. The reviewer will determine if information labeled "n/a" is required and whether information must be submitted.
- 3. Those items noted with an "asterisk" are not typically required for conceptual/ preliminary report. Applicant shall confirm this with local jurisdiction.
- 4. Submit three (3) copies of report and include copy of check list bound with report.

TITLE PAGE

- A. Type of report (Conceptual/Preliminary or Final Drainage Report).
- B. Project Name.
- C. Preparer name, firm, address, number, and date.
- D. Professional Engineer's seal of preparer.
- E. Certifications (see SWMM Section 303.1)

I. INTRODUCTION

- A. Background
 - 1. Identify report preparer and purpose.
 - Identify date of letter with previous County comments.

B. Project Location

- 1. Identify Township, Range, and Section.
- 2. Identify adjacent street and subdivision names.
- 3. Reference to General Location Map.

C. Property Description

- 1. Identify area in acres of entire contiguous ownership.
- 2. Describe existing ground cover, vegetation, soils, topography and slopes.
- 3. Describe existing drainage facilities, such as channels, detention areas, or structures.
- 4. Describe existing irrigation facilities, such as ditches, head-gates, or diversions.
- Identify proposed types of land use and encumbrances.

D. Previous Investigations

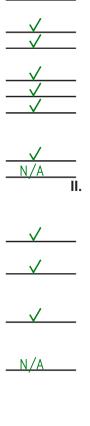
- 1. Identify drainage master plans that include the project area, including floodplain studies.
- Identify drainage reports for adjacent development.

DRAINAGE SYSTEM DESCRIPTION

- A. Existing Drainage Conditions
 - 1. Describe existing topography and provide map with contours extending a minimum of 100 feet beyond property limits.
 - 2. Identify major drainageway or outfall drainageway and describe map showing location of proposed development within the drainageways.
 - 3. Identify pre-developed drainage patterns and describe map showing predeveloped sub-basins and concentrated discharge locations. Provide calculations of pre-developed peak flows entering and leaving the site.

B. Master Drainage Plan

- 1. Describe location of the project relative to a previously prepared master drainage plan, including drainage plans prepared for adjacent development.
- C. Offsite Tributary Area



,		
		 Identify all offsite drainage basins that are tributary to the project.
		2. Identify assumptions regarding existing and future land use and effects of offsite
/		detention on peak flows.
	D.	Proposed Drainage System Description
	٥.	Identify how offisite stormwater is collected and conveyed through the site and
,		
		ultimately to the receiving water(s).
		2. Identify sub-basins and describe, in general terms, how onsite stormwater is
		collected and conveyed through the site for each location where stormwater is
		discharged from the site.
*		3. Describe detention volumes, release rates and pool elevations.
		4. Identify the difference in elevation between pond invert and the groundwater
√ *		table.
		5. Describe how stormwater is discharged from the site, including both
1		concentrated and dispersed discharges and rates.
		6. Describe stormwater quality facilities.
*		
		7. Describe maintenance access aspects of design.
, a.		8. Describe easements and tracts for drainage purposes, including limitation on
*	_	use.
	E.	Drainage Facility Maintenance
		1. Identify responsible parties for maintenance of each drainage and water quality
*		facility.
*		Identify general maintenance activities and schedules.
III.	DR	AINAGE ANALYSIS AND DESIGN CRITERIA
	Α.	Regulations
		1. Identify that analysis and design was prepared in accordance with the
√		provisions of the Manual.
		 Identify other regulations or criteria which have been used to prepare analysis
. /		and design.
	B.	
	D.	Development Criteria
		1. Identify drainage constraints placed on the project, such as by a major
,		drainage study, floodplain study or other drainage reports relevant to the
		project.
		2. Identify drainage constraints placed on the project, such as from major street
<u> N/A</u>		alignments, utilities, existing structures, and other developments.
	C.	Hydrologic Criteria
		(If Manual was followed without deviation, then a statement to that effect is all
		that is required. Otherwise provide the following information where the criteria
		used deviates from the Manual.)
		1. Identify developed storm runoff peak flows and volumes and how they were
1		determined, including rainfall intensity or design storm.
		2. Identify which storm events were used for minor and major flood analysis and
. /		design.
		
	_	Identify how and why any other deviations from the Manual occurred.
	D.	Hydraulic Criteria
		(If Manual was followed without deviation, then a statement to that effect is all
		that is required. Otherwise provide the following information where the criteria
		used deviates from the Manual.)
		1. Identify type(s) of streets within and adjacent to development and source for
*		allowable street capacity.
		2. Identify which type(s) of storm inlets were analyzed or designed and source for
✓ *		allowable capacity.
		3 Identify which type of storm sewers which were analyzed or designed and

*	Manning's n-values used.
	4. Identify which method was used to determine detention volume requirements
*	and how allowable release rates were determined.
N/A*	5. Identify how the capacity of open channels and culverts were determined.
	6. Identify any special analysis or design requirements not contained with the
N/A*	Manual.
	7. Identify how and why any other deviations from the Manual occurred.
,	E. Variance from Criteria
	Identify any provisions of the Manual for which a variance is requested.
****	2. Identify pre-existing conditions which cause the variance request.
*IV.	POST CONSTRUCTION STORMWATER MANAGEMENT. See Manual Section 1600
	for requirements. Note: This section of the Final Drainage Report identifies additional information required by
,	Note: This section of the Final Drainage Report identifies additional information required by Mesa County's, City of Grand Junction's, and Town of Palisade's, Permit for
	Stormwater Discharges Associated with Municipal Separate Storm Sewer Systems
	(MS4s), permit No. COR-090000. The Final Drainage Plan and the Construction
	SWMP (see SWMM Section 1500) meets the requirements of the MS4s Permit. In
	general, this section identifies permanent BMP practices to control the discharge of
	pollutants after construction is complete.
	*A. Stormwater Quality Control Measures
	Describe the post-construction BMPs to control discharge of pollutants from the
N/A*	project site.
	2. If compensating detention is provided, discuss practices to address water
<u>N/A</u> *	quality from area not tributary to detention area.
•	3. If underground detention is proposed, discuss how water quality facilities will be
<u>N/A</u> *	provided on the surface.
	4. If proprietary BMPs are proposed, provide the justification and sizing
<u> N/A</u>	requirements (see SWMM Section 1603.3).
	*B. Calculations
,	1. Provide methods and calculations for WQCV, sediment storage, and water
	quality outlet structure.
V.	CONCLUSIONS
	A. Compliance with Manual
,	Compliance with Manual and other approved documents, such as drainage plans and floodplain studies.
	B. Design Effectiveness
./	Effectiveness of drainage design to control impacts of storm runoff.
	C. Areas in Flood Hazard Zone
	Meet requirements of Floodplain Regulations: Mesa County Land Development
/	Code, Section 7.13; City of Grand Junction Zoning and Development Code,
	Section 7.1.
	D. Variances from Manual
	Applicant shall identify any requested variances and provide basis for approving
	variance. If no variances are requested, applicant shall state that none are
	requested.
VII.	REFERENCES
	Provide a reference list of all criteria, master plans, drainage reports, and technical
	information used.
,	TABLES
	Include copy of all tables prepared for report.
,	FIGURES
	A. General Location Map (See Section 303.2a)

	B. Flood Plain InformationC. Drainage Plan (See Section 303.2b)D. Other pertinent figures.
	A. DESIGN CHARTS 1. Provide copy of all design charts (i.e.: tables, figures, charts from other criteria) used for the report. B. HYDROLOGIC CALCULATIONS (see Manual Sections 600 and 700) 1. Land use assumptions for off-site runoff calculations. 2. Time of concentration and runoff coefficients for pre-existing and post development conditions. 3. Pre-developed hydrologic computations. 4. Developed conditions hydrologic computations. C. HYDRAULIC CALCULATIONS 1. Capacity of existing channels, streets, storm sewers, inlets, culverts and other facilities. 2. Calculations for existing storm sewer and open channel. 3. Irrigation ditch flows and ditch system capacity. 4. Detention pond design (see Manual, Section 1400 for requirements). a. Storage volume, release rates, and pool elevations for 10-year and 100-year storm. b. Outlet structure dimensions, orifice diameter, weir lengths, pipe headwater and other data. c. Outlet velocity and energy dissipation requirements. d. Routing of outlet flows and emergency spillway flows. 5. Street capacity calculations, if data in Manual not used (see Section 1100). 6. Storm inlet capacity calculations, if data in Manual not used (see Section 1100).
*****	 Storm sewer capacity calculations, if data in Manual not used (see Section 1000). Channel capacity calculations, if data in Manual not used (see Section 800). Culvert capacity calculations (see Manual, Section 1200). Other hydraulic structure calculations (see Manual, Section 900). STORMWATER QUALITY CALCULATIONS Water Quality Capture Volume (WQCV). Storage volume for sediment volume and pool elevations for WQCV. Outlet calculations for required area per row, diameter of individual holes, number of holes per row, and number of holes per column. CERTIFICATION – PROFESSIONAL ENGINEER'S SEAL AND SIGNATURE Craig Rothluebber, PE

Table 303 Stormwater Management Manual Drainage Plan Checklist

Instructions:

- 1. Applicant to identify with a "check-mark" if information is provided. If applicant believes information is not required, indicate with "n/a".
- 2. County will determine if information labeled "n/a" is required and whether information must be submitted.

I. EXISTING FACILITIES

- A. Contours at two foot intervals, based on USGS datum. Contours to extend at least 50 feet past property line.
 - B. Location and elevation of USGS benchmarks or benchmarks referenced to USGS.
 - C. Property lines.
 - D. Drainage easements.
 - E. Street names.
 - F. Major and minor channels and floodplains.
 - G. A historic drainage plan including historic basin boundaries and flow paths.

II. PROPOSED FACILITIES

- A. Contours at two-foot intervals, based on USGS datum.
- B. Property lines.
- C. Drainage easements.
- D. Street names and grades.
- E. Right of way and easement.
- F. Finished floor elevations for protection from major storm run-off.
- G. Detention pond information:
 - 1. Location of each detention pond with site at 1"=50' scale or larger with 2-foot contour intervals.
 - 2. Inlet and outlet structure, and trickle channel design details.
 - 3. Details of emergency spillway and channel.
 - 4. Landscape information, including side slopes, vegetation and planting requirements.
 - 5. Details of water quality outlet structure.
- H. Channel Information:
 - 1. Profiles with existing and proposed grades.
 - 2. Cross sections on 100-foot stations showing existing and proposed topography and required rights of way.
 - 3. Locations and size of all existing and proposed structures.
 - 4. Locations and profiles of adjacent utilities.
 - 5. Typical channel section and lining details.
- I. Storm sewer information:
 - 1. Alignment and location of manholes, inlets, and outlet structures.
 - 2. Profile of invert and pipe crown.
 - 3. Invert elevations at manholes and inlets.
 - 4. Lengths and grades between manholes and inlets.
 - 5. Locations and elevations of utilities adjacent to and crossing storm sewer.
 - 6. Easement and other O&M access geometry.
 - 7. Outlet details, such as end sections, headwall and wingwalls, erosion control, and vegetation.
- J. Street cross sections with design 100-year flood depth.
- K. Other drainage related structures and facilities, including underdrains and sump pump discharge lines.
- Other permanent BMP measures to control pollutant discharges to the County's MS4 system.



 $\sqrt{\text{(see plans)}}$ $\sqrt{\text{(see plans)}}$

 $\sqrt{\text{(see plans)}}$

 $\sqrt{\text{(see plans)}}$

N/A

N/A √(see plans) N/A N/A

 $\frac{\sqrt{\text{(see plans)}}}{\sqrt{\text{(see plans)}}}$

 $\sqrt{\text{(see plans)}}$ $\sqrt{\text{(see plans)}}$ $\sqrt{\text{(see plans)}}$

 $\frac{\sqrt{\text{(see plans)}}}{\sqrt{\text{(see plans)}}}$

N/A N/A

	III.	HYDRAULIC AND HYDROLOGIC INFORMATION
		A. Routing and accumulative runoff peaks at upstream and downstream ends of the sit
		and at various critical points onsite for initial and major storms. Inflow and outflo
✓		from each subbasin shall be shown for both initial and major storms.
$\sqrt{\text{(see plans)}}$		B. Street cross sections showing 100-year flood levels.
		C. Major and minor channels and floodplains.
		D. Detention pond data:
		1. Release rates for 10- and 100-year storm events.
		Required and provided volumes for 10- and 100-year storm events.
		Design depths for 10- and 100-year storm events.
		Water quality capture volume and pool elevation.
		E. Channel data:
<u> </u>		Water surface profiles.
<u> </u>		Representative 100-year flow velocity and Froude number.
		F. Storm sewer data:
		Profile of water surface for design flow rate.
		2. Peak flows for design flow, 2-year and 100-year storm events.
	IV.	STANDARD NOTES
		A. No building, structure, or fill will be placed in the detention areas and no changes
,		alterations affecting the hydraulic characteristics of the detention areas will be made
		without the approval of the County.
		B. Maintenance and operation of the detention and water quality areas is the
		responsibility of property owner. If owner fails in this responsibility, the County ha
. /		the right to enter the property, maintain the detention areas, and be reimbursed for costs incurred.
		C. Detention pond volumes, all drainage appurtenances, and basin boundaries shall be
		verified. As-built drawings shall be prepared by a registered professional engine
1		prior to issuance of certificate of occupancy for any structure within the development
		D. Permission to reproduce these plans is hereby given to Mesa County for County
		purposes associated with plan review, approval, permitting, inspection an
		construction of work.
✓	V.	PROFESSIONAL ENGINEER'S SEAL AND SIGNATURE
<u> </u>	VI.	OTHER
$\sqrt{\text{(see plans)}}$		A. Horizontal and vertical control information and ties to existing and proposed features
,	ACI	KNOWLEDGEMENTS
		Drainage Plan checklist was prepared by: