# FINAL DRAINAGE REPORT

## SANTA FE RANCH SUBDIVISION

## FRUITA, COLORADO

#### PREPARED FOR:

Mr. John Folkestad 1255 Q Road Loma, CO 81524 (970) 858-1436

### PREPARED BY:

## VISTA ENGINEERING CORP.

2777 Crossroads Blvd. Grand Junction, CO 81506 (970) 243-2242

> September 24, 2003 VEC # 4107.02-02

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## **CERTIFICATION**

I hereby certify that this Final Drainage Report for Santa Fe Ranch Subdivision was prepared under my direct supervision.

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Patrick M. O'Connor, P.E. Registered Professional Engineer State of Colorado, # 20759

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## FINAL DRAINAGE REPORT SANTA FE RANCH SUBDIVISION

#### I. LOCATION AND DESCRIPTION OF PROJECT

Santa Fe Ranch Subdivision is located approximately 1/8 mile north of K Road along the east side of Big Salt Wash. The Sketch-Plan was approved earlier this year and the project is currently within the Fruita City limits zoned "Community Residential". The project is comprised of one Mesa County Tax parcel (number 2697-074-00-046) containing 9.691 acres. This is a request for Preliminary-Final Plan approval.

The proposed project will ultimately consist of 26 single-family residential lots for an overall density of 2.68 units per acre. Included are 2.920 acres of open-space (30.1% of total area) to be dedicated to the City of Fruita for various uses including public trails.

Existing streets in the vicinity include Juniper Street adjacent immediately to the east, and Ponderosa Drive which exists in the Orchard Valley subdivision immediately adjacent to the south. Urban residential streets are capable of being extend into the adjacent parcel to the east to provide neighborhood connectivity. All streets and utilities will be constructed in conformance with current City of Fruita Standards and Specifications. The project will be designed to comply with the standards listed in the current City of Fruita Development Code for "Community Residential" zoning.

The site is currently vacant and being utilized as flood-irrigated pasture. Access to the project will occur initially from the Juniper Street entrance, but can also be accomplished from the east once the adjacent parcel is developed. Disturbance of the open space tract will be minimal in an attempt to minimize impacts on the natural vegetation and wildlife of the Big Salt Wash. Irrigation of the developed area, especially along the bank of Big Salt Wash, will be restricted to aid soil stability of the bank and to accommodate peak watering demands with available water. Ownership of the open space tract will be dedicated to the City. The landscaping, and maintenance, of all single family lots will be the responsibility of individual lot owners.

The soils at the site have been evaluated by a geotechnical analysis included within Final Plan submittal and are typical for the Fruita area. The surface soils generally consist of lean clays, sandy silts, and silty sand. These soils are categorized as hydrologic soils group "B" which have low to moderate infiltration capability and moderate runoff potential. This should not pose an adverse impact to development of the site. There are no known geological hazards at this location which would preclude site development as planned, provided the engineering recommendations of the construction drawings and the Subsurface Exploration Report are followed.

#### II. EXISTING DRAINAGE CONDITIONS

#### **MAJOR BASIN**

Santa Fe Ranch is located in northwest Fruita within the major basin of the Big Salt Wash. Contours on topographic maps of the site included in the appendix show that the site drains directly to the Big Salt Wash, which ultimately drains into the Colorado River approximately ½ mile downstream.

The developed portions of Santa Fe Ranch do not exist within the designated 100 year floodplain of the Big Salt Wash, Colorado River Basin, or any other basin as delineated by the July 15, 1992 Flood Insurance Rate Maps produced by FEMA. The 100 year floodplain, per these maps, does exist along the Big Salt Wash, but is contained below the upper bank and is not within the area designated for residential construction.

#### SITE

Topography of the property is relatively "flat" in nature, sloping generally southwest at an average rate of less than one percent. Pasture grasses cover most of the site with gated-pipe providing irrigation delivery and tail-water being collected around the perimeter by surface ditches. Irrigation is delivered to the property by a Grand Valley Irrigation Company pipeline existing in the northeast corner of the site. Runoff from the site has historically flowed south to be collected by a tailwater ditch along the southern boundary. This ditch flows west to an existing drain pipe in the southwest corner which discharges stormwater runoff and irrigation return flows directly into the Big Salt Wash.

#### OFF-SITE IMPACTS TO THE SITE

Offsite surface runoff in the vicinity is collected and diverted away from the site by the existing topography and surface ditches surrounding the project. Existing topography of the area can been seen from maps in the appendix to drain generally south and west, toward Big Salt Wash and the river. The wash exists generally along the north and west boundaries, providing a collection barrier from the north. The property to the east drains to the south, not to the west, along the common boundary with Santa Fe Ranch and, therefore, does not impact the site. An existing subdivision (Evening Breeze) exists immediately south of the site which contains and discharges runoff directly to the Big Salt Wash through its own system of streets and stormwater management.

### III. PROPOSED DRAINAGE CONDITIONS

#### **CHANGES IN DRAINAGE PATTERNS**

No major change in the released drainage pattern is proposed for the site. Drainage patterns within the site will be modified to accommodate development and to better control surface flows to designated collection areas. Development of the site will eliminate flood-irrigation practices through the installation of a pressurized irrigation system delivering water to each lot for distribution to small individual lawns. Upon development, runoff will flow into the streets to be collected and directed for direct-discharge into the Big Salt Wash near the southwest corner of the site, where it has historically drained

Improvements are proposed for the discharge location to prevent erosion. Once the runoff reaches the low-point in the streets (near the southwest corner) it will be carried by a concrete channel/walkway to the bank of the wash. Here it will be discharged into an underground pipeline to transport flows to the wash, under proposed walking trails in the open-space.

#### **MAINTENANCE**

Access to the stormwater management improvements will be by platted streets and easements as required. A Home Owners Association will be formed to provide maintenance responsibility for the surface improvements related to the facility. Operation and maintenance of the future underground storm sewers will ultimately be the responsibility of the City of Fruita.

#### IV. DRAINAGE DESIGN CRITERIA AND APPROACH

#### **REGULATIONS**

The City of Fruita Stormwater Management Master Plan (SWMMP - June, 1998) and Mesa County Stormwater Management Manual (SWMM - May, 1996) were used as the basis for analysis and facility design criteria. No other master drainage plan has been completed for the area, to our knowledge. This development was designed within the guidelines of the SWMMP and the SWMM to assure minimal impacts to downstream properties.

#### HYDROLOGICAL CRITERIA

Because the project is a residential development containing sub-basins less than 25 acres, the "Rational Method" was used to calculate the historic and developed flow rates. As required, a minor storm is considered to be a 2-year frequency and a major storm is considered to be a 100-year frequency event.

Runoff Coefficients and intensity-duration-frequency data used in the computations were based on the most recent SWMM criteria defined above. Coefficients were assigned based on land use and hydrologic soils group. Haestad Methods software ("Pondpack") was used to perform the calculations.

#### **HYDRAULIC CRITERIA**

All site facilities and conveyance elements were designed in accordance with the City of Fruita SWMMP and the City of Fruita Design Standards and Construction Specifications.

The design includes a concrete channel/walkway and a section of 15" RCP pipeline to carry water from the street to the discharge location in the wash. Open channels and pipelines were analyzed using Manning's Equation and roughness coefficients found in the SWMM Manual. Haestad Flowmaster Software was used to perform the calculations. Copies of these calculations are included in the appendix.

#### **DIRECT-DISCHARGE (DRAINAGE IMPACT FEE)**

A calculation of the DRAINAGE IMPACT FEE follows. It is based on the composite "C" values calculated in the appendix and the formula contained within the Fruita SWMMP manual.

\$FEE = \$12,000 ( 
$$C_{d100} - C_{h100}$$
) A <sup>0.7</sup>  
= \$12,000 (0.36 - 0.25) 9.691 <sup>0.7</sup>  
= \$6,471.90

#### V. RESULTS AND CONCLUSION

#### **AREAS**

Site (Total)

9.70 Acres

#### **RUNOFF COEFFICIENTS - "C"**

Big Salt Wash area	- 0.18 (2 yr.)	0.21 (100 yr.)
Pasture	- 0.22 (2 yr.)	0.27 (100 yr.)
Developed (¼ ac./unit)	- 0.33 (2 yr.)	0.42 (100 yr.)

#### TIMES OF CONCENTRATION

Historic Site

32 minutes

Developed Site

20 minutes

#### **RUNOFF** (All Flows are cubic-feet per second)

	Historic	lotal
	Site (Undeveloped)	Site (Developed)
2 Year	1.05	1.89
100 Year	4.98	9.32

#### **CONCLUSION**

The developed site will direct-discharge runoff into the Big Salt Wash at rates greater than the historic rates, but generally in the same location. No detention is proposed for developed runoff from this site, therefore a Drainage Impact Fee has been calculated. Irrigation return flows from the site should be greatly reduced by the elimination of furrow irrigation and the implementation of reduced landscaping and watering restrictions.

### **APPENDIX**

#### 1. SITE MAPS

Santa Fe Ranch - Grading and Drainage Plan
Santa Fe Ranch - Stormwater Management Plan
Vicinity Topography Map - Mesa County Mapping
Major Basin Drainage Map (partial U.S.G.S. Quad Sheet - Fruita)

#### 2. COEFFICIENTS

Runoff "C" Values (Rational Formula) Composite "C" Value Calculations Drainage Impact Fee Calculation

## 3. <u>TIMES OF CONCENTRATION</u>

Summary
Existing Site (HISTORIC)
Existing Site (DEVELOPED)

### 4. RUNOFF

SITE - Historic - 2 Year & 100 Year SITE - Developed - 2 Year & 100 Year

### 5. **HYDRAULICS**

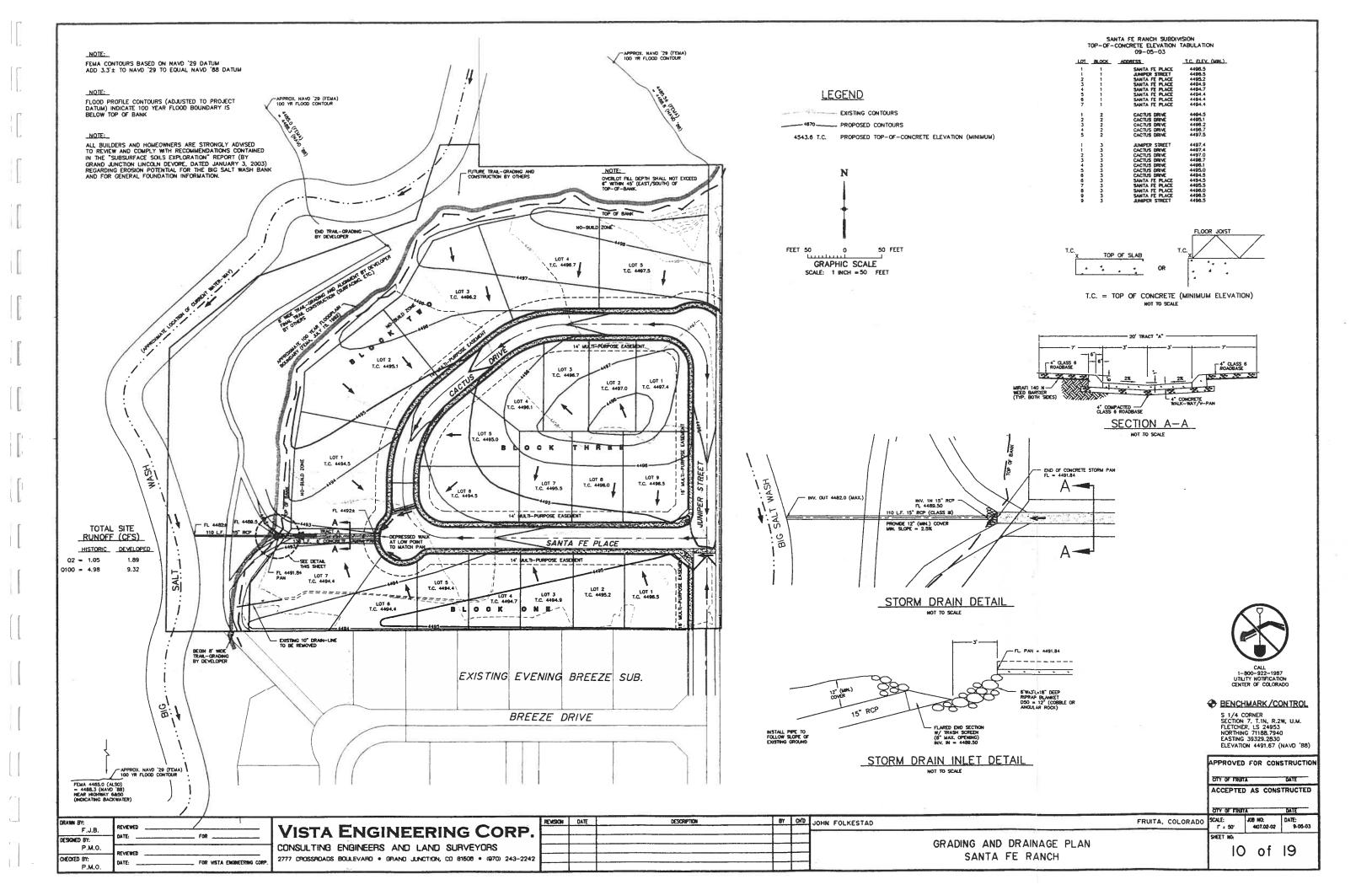
Storm Outlet Channel - Capacity Calculation

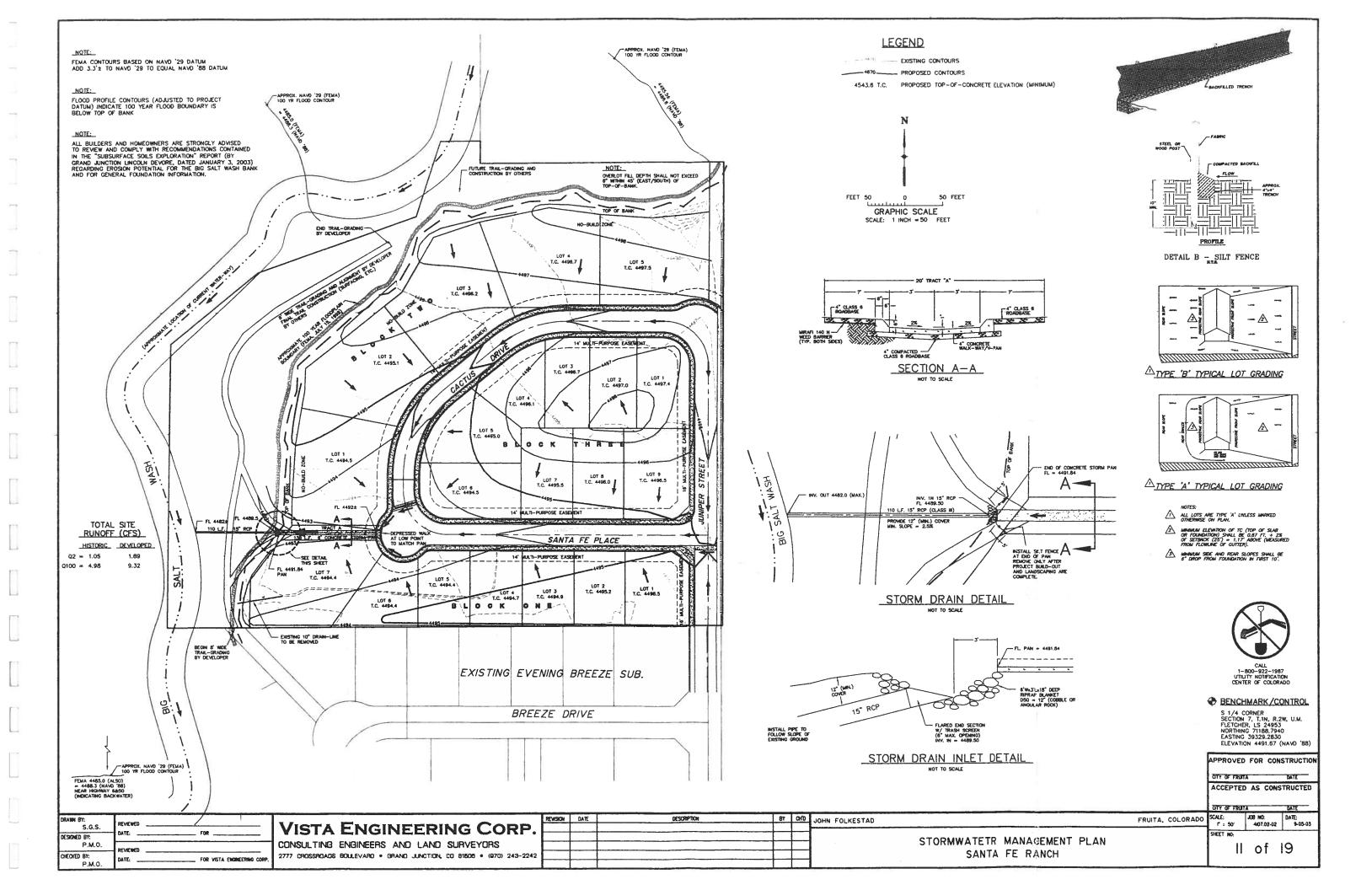
Storm Outlet Channel - Cross-Section

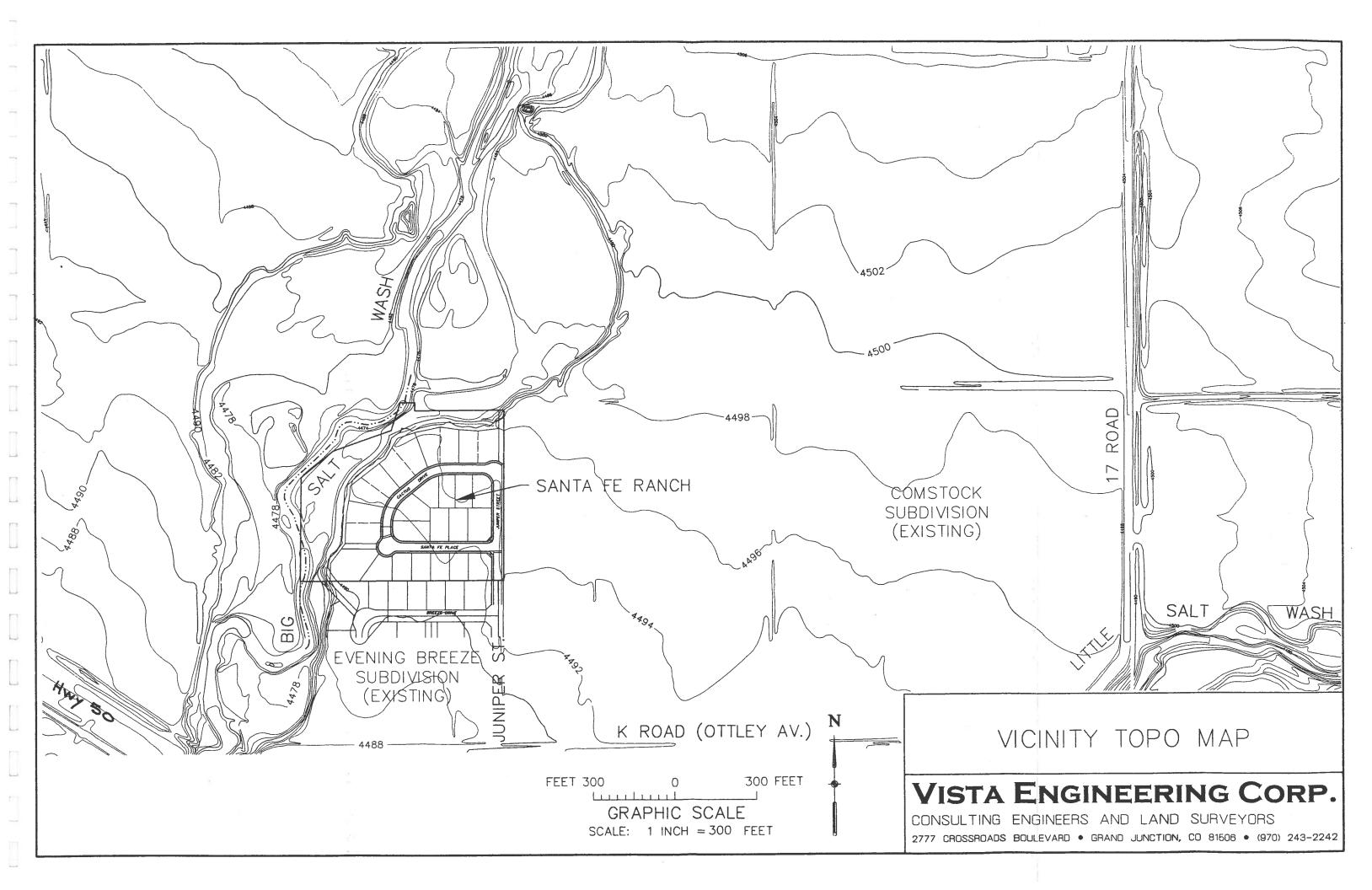
Storm Outlet Pipeline - Capacity Calculation

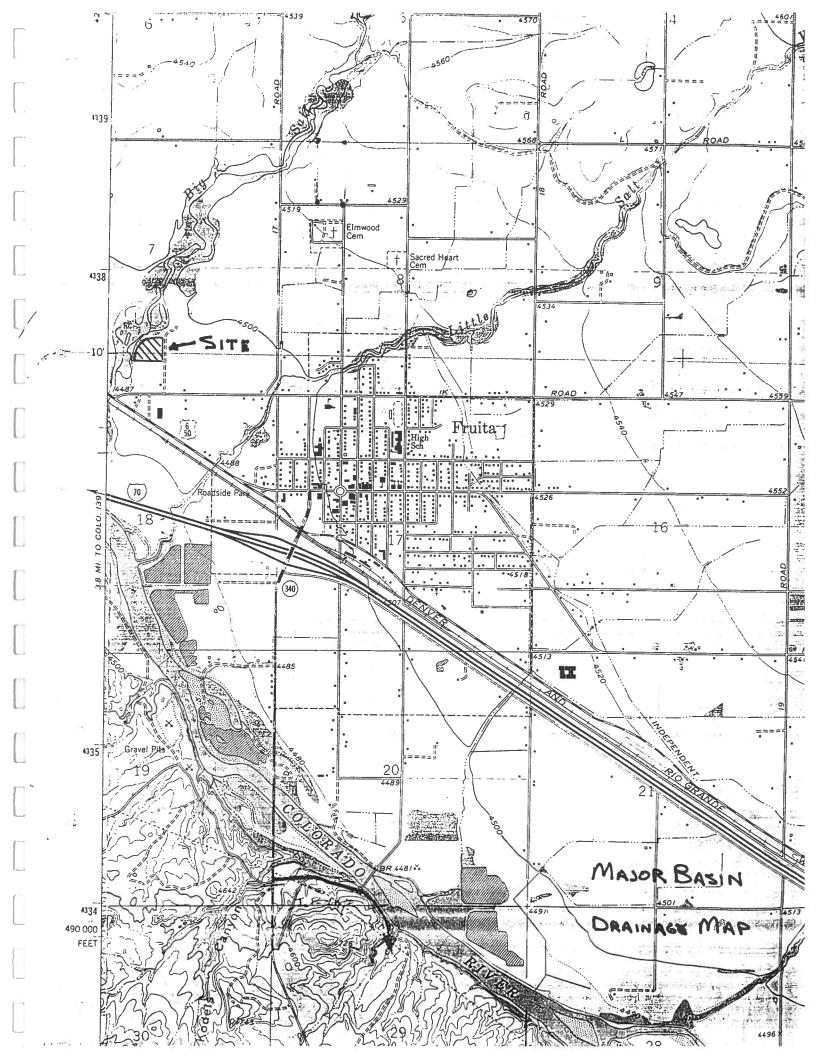
Storm Outlet Pipeline - Rating Table for varied hydraulic slopes

SECTION 1 SITE MAPS









SECTION 2 COEFFICIENTS

0.33 0.47 0.33 0.47	
t <sub>ن</sub> ا	
PASTURE WASH/DENSE DEVELOPEO	
FASTUR WASH, DEVELO	

LAND USE OR		SCS	HYDRO	SCS HYDROLOGIC SOIL GROUP (SFF	OIL GRC	TIP (SFE		"" XIC	EOD DE	APPENDIY "C" FOB DESCRIPTIONS	MC	
CITADACTEDICTICE		A			g			7 7	LOW DE.	CMFTIC	(CNI	
CHAICACLEMBILCS					<u>-</u>		The name of some contract of	ပ				
	0.5%	7-6%	+%9	0.2%	7-6%	+%9	0-2%	7-6%	+%9	0-2%	2-6%	+%9
UNDEVELOPED AREAS Bare ground	10 - 20	.1626	.2535	14 - 22	22 - 30	.3038	87 .07:	28-36	3644	24-32	.3038	.4048
Cultivated/Agricultural	T 08 - 18 =	.13	.1626	11 ST 19	.15	21 - 29	14-22	.19 - 27	.2634	26	.2331	.3139
Pasture	12: 22	25-	.3040	18 25	34	.3745		34.42	.4452	30 :38	.40 - 48	.5058
Meadow	#10=20 14=24	.16-	.2535	14   22 20   28	1 1 1	30-38	1-1	28 - 36	.3644	24-45	30 - 38	.4048
Forest	05 15 15 18 18 18 18 18 18 18 18 18 18 18 18 18	-08-	1 1 1	10.18 10.18	111 1	14 - 22	The inte	13-21	.1624	20 2	.1624	20 - 28
RESIDENTIAL AREAS 1/8 acre per unit	40 - 50	.4353	.4656	42~ 50 30~38*		50 - 58		.4856	19 62.	2) S	.5159	25-33
1/4 acre per unit	27 37	39-	.3444	29 - 37 38 - 46	34 - 42	38 - 46		3644	.4149	4 6	.3947	.4553
1/3 acre per unit	100 Hz	26- 35-	.2939	25 2 53		.3341		32 - 40	3745	31.39	11 6	11 1
1/2 acre per unit	16-76 25-95	29.0		19 - 27 28 - 36		i		27-35			• i •	.3361
1 acre per unit	14 34	.1926	22 - 32	83 1/4	i • •	.26 - 34		1 1	31 - 39		29 - 37	.3543
MISC. SURFACES Pavement and roofs	.93	.94 96	26. 70.	93	96	\$6. 70		94	.95	86	.94	.4654
Traffic areas (soil and gravel)	\$5=:65 65=:70	.6070 .7075	.7479	60 68 68 76	.6472	67 - 75	64 72	2773.	7769.	72= 80	.75 - 83	
Green landscaping (lawns, parks)	10.20	.16 - 26	.25 - 35	14 22 20 28	22 - 30	30-38	1 1 1	28 - 36	.3644	24 92	30 - 38	.4048
Non-green and gravel landscaping	30 : 40	.36 - 46	.45 - 55	45-55 30-60	.42 . 50	.50 - 58		.48 . 56	.5664	8. 1 4. 8. 71	50 - 58	.5058
Ceneteries, playgrounds	20 30	.26 - 36	.3545	35 45	32 - 40	40 - 48		3844	1		89:-09:	.5058
NOTES: 1. Values above and below pertain to the 2-year and 100-year storms, respectively.  The range of values provided allows for engineering judgement of site conditions atorm duration. In general, during shorter duration storms (Tc < 10 minutes), use a ""C value in the higher range. For residential development of less than 100, no a ""C value in the higher range.	and below perfalues provided. In general, of ation storms (development)	aln to the 2-3 if allows for e luring shorte Ic ) 30 minut	year and 100- inglicering h ir duration st (es), use a ""(	te 2-year and 100-year storms, respectively. for engineering Judgement of site condition horter duration storms (Tc < 10 minutes), use a ""C value in the higher rang	respectively.  of minutes), in  thigher range	s such as bas iffiltration ca	ic shape, hon	ogenetty of s	urface type,	he 2-year and 100-year storms, respectively.  for engineering judgement of site conditions such as basic shape, homogeneity of surface type, surface depression storage, and horter duration storas (Tc < 10 minutes), infiltration capacity is higher, allowing use of a "C" value in the higher range. Conversely house a "C" value in the higher range.	.3058   ssion storage w range. Co.	00 10 10
SURFACES to estimale "C" value ranges for use	estimale "C"	value range	for use.	un or grence.	r man 1 acre	per unit, and	also for com	mercial and	Industrial ar	man no acter. Impes for use.	s under MIS	C

RATIONAL METHOD RUNOFF COEFFICIENTS (Modified from Table 4, UC-Davis, which appears to be a modification of work done by Rawls)

TABLE "B-1"

Quick TR-55 Ver.5.46 S/N: Executed: 21:24:30 09-04-2003

SANTA FE RANCH SUBDIVISION
JOHN FOLKESTAD - FRUITA, CO
COMPOSITE "C" VALUES
9/1/03

"C" VALUE
RUNOFF CURVE NUMBER SUMMARY

"C" VALUE Subarea Area Description (acres) (weighted) \_\_\_\_\_ HIST SITE 2 YR 9.70 0.21 9.70 0.25 HISTORIC 100 YR 9.70 DEV. SITE 2 YR 0,29 9.70 0.36 DEV SITE 100 YR

Executed: 21:24:30 09-04-2003

# SANTA FE RANCH SUBDIVISION JOHN FOLKESTAD - FRUITA, CO COMPOSITE "C" VALUES 9/1/03

RUNOFF CURVE	NUMBER DATA	

Composite Area: HIST SITE 2 YR

SURFACE DESCRIPTION	AREA (acres)	CN	
FURROW IRRIGATED FIELD BIG SALT WASH - DENSE VEG.	6.90 2.80	22 18	
COMPOSITE AREA>			( 21 )

Composite Area: HISTORIC 100 YR

SURFACE DESCRIPTION	AREA (acres)	CN	
FURROW IRRIGATED FIELD BIG SALT WASH - DENSE VEG.	6.90 2.80	27 21	
COMPOSITE AREA>	9.70	25.3	( 25 )

Composite Area: DEV. SITE 2 YR

SURFACE DESCRIPTION	AREA (acres)	CN	
DEVELOPED AREA - 1/4 AC/UNIT BIG SALT WASH - DENSE VEG.	6.90 2.80	33 18	
COMPOSITE AREA>	9.70	28.7	(29)

Quick TR-55 Ver.5.46 S/N: Executed: 21:24:30 09-04-2003

Composite Area: DEV SITE 100 YR

SURFACE DESCRIPTION	AREA (acres)	CN	
DEVELOPED AREA - 1/4 AC/UNIT BIG SALT WASH - DENSE VEG.	6.90 2.80	42 21	
COMPOSITE AREA>	9.70	35.9	(36)

# SECTION 3 TIMES OF CONCENTRATION

Executed: 20:58:13 09-04-2003 SANTA FE.TCT

SUMMARY SHEET FOR Tc or Tt COMPUTATIONS (Solved for Time using TR-55 Methods)

SANTA FE RANCH SUBDIVISION HISTORIC AND DEVELOPED Tc's 9/01/03

Subarea descr.	Tc or Tt	Time (hrs)	
HISTORIC SITE	Tc	0.53 =	ZZ MINNYES
DEVELOPED SITE	Tc	0.33 =	20 MINUTES

Executed: 20:58:13 09-04-2003 SANTA FE.TCT

SANTA FE RANCH SUBDIVISION HISTORIC AND DEVELOPED Tc's 9/01/03

Tc COMPUTATIONS FOR: HISTORIC SITE

SHEET FLOW (Applicable to Tc only)		_			
Segment ID	D3.00	1			
Surface description Manning's roughness coeff., n	PAST				
Flow length, L (total < or = 300)	ft	0.0300			
Two-yr 24-hr rainfall, P2					
Land slope, s	f+ / f+	0.700 0.0050			
0.8	10/10	0.0050			
.007 * (n*L)					
T =	hrs	0.40		=	0.40
0.5 0.4					0.40
P2 * s					
SHALLOW CONCENTRATED FLOW					
Segment ID		2			
Surface (paved or unpaved)?		Unpaved			
Flow length, L		500.0			
Watercourse slope, s	ft/ft	0.0050			
0.5					
0.5 $Avg.V = Csf * (s)$	e/	1 1400			
where: Unpaved Csf = 16.1345	It/s	1.1409			
Paved Csf = 20.3282					
raveu CS1 - 20.3282					
T = L / (3600*V)	hrs	0.12		_	0.12
/ (3333 )/		0.12		_	0.12
CHANNEL FLOW					
Segment ID					
Cross Sectional Flow Area, a	sq.ft	0.00			
Wetted perimeter, Pw	ft	0.00			
Hydraulic radius, $r = a/Pw$	ft	0.000			
Channel slope, s	ft/ft	0.0000			
Manning's roughness coeff., n		0.0000			
2/2 1/2					
2/3 1/2 1.49 * r * s					
V =	£L /-	0 0000			
n	ft/s	0.0000			
11					
Flow length, L	ft	0			
		· ·			
T = L / (3600*V)	hrs	0.00		=	0.00
					3.00
	::::::	:::::::::	:::::::::::::::::::::::::::::::::::::::	:::	::::::
		TOTAL TI	ME (hrs)		0.53
			•		

Executed: 20:58:13 09-04-2003 SANTA FE.TCT

SANTA FE RANCH SUBDIVISION HISTORIC AND DEVELOPED Tc's 9/01/03

TC COMPUTATIONS FOR: DEVELOPED SITE

SHEET FLOW (Applicable to Tc only) Segment ID Surface description	LAWN	1			
Manning's roughness coeff., n		0.0450			
Flow length, L (total < or = 300	) ft	120.0			
Two-yr 24-hr rainfall, P2	in	0.700			
Land slope, s	ft/ft				
0.8	10/10	0.0100			
.007 * (n*L) T =	hwa	0 20			0 00
_	hrs	0.20		=	0.20
0.5 0.4					
P2 * s			每		
SHALLOW CONCENTRATED FLOW Segment ID					
Surface (paved or unpaved)?					
Flow length, L	ft	0.0			
Watercourse slope, s	ft/ft	0.0000			
0.5					
Avg.V = Csf * (s) where: Unpaved Csf = 16.1345 Paved Csf = 20.3282	ft/s	- 0.0000			
T = L / (3600*V)	hrs	0.00			0.00
CHANNEL FLOW					
Segment ID		2			
Cross Sectional Flow Area, a	sq.ft	4.00			
Wetted perimeter, Pw	ft	24.00			
Hydraulic radius, $r = a/Pw$	ft	0.167			
Channel slope, s	ft/ft				
Manning's roughness coeff., n	10/10	0.0160			
maining s roughness coerr., if		0.0100			
2/3 1/2 1.49 * r * s					
V =	ft/s	1.9943			
n	,				
Flow length, L	ft	900			
· - · · · · - · · · · · · · · · · · · ·		2 2 3			
T = L / (3600*V)	hrs	0.13		=	0.13
		TOTAL T	::::::::: IME (hrs)	:::	0.33

SECTION 4 RUNOFF Quick TR-55 Ver.5.46 S/N: Executed: 22:05:19 09-04-2003

> SANTA FE RANCH SUBDIVISION - FRUITA HISTORIC RUNOFF - TOTAL SITE 9/1/03

\* \* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 2 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

				=	==:		======	=======	======
Subarea Descr.	Runoff 'C'	Area acres	Tc: (min)	Wtd. 'C'		Adj. 'C'	I in/hr	Total acres	Peak Q (cfs)
PASTURE WASH/DENSE	0.220 0.180	6.90 2.80							
			32.00	0.208		0.208	0.520	9.70	1.05

Executed: 22:05:19 09-04-2003

#### SANTA FE RANCH SUBDIVISION - FRUITA HISTORIC RUNOFF - TOTAL SITE 9/1/03

\* \* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years 'C' adjustment, k = 1.1905 Adj. 'C' = Wtd.'C' x 1.1905

				:	==		======	=======	=======
Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd. 'C'		Adj. 'C'	I in/hr	Total acres	Peak Q (cfs)
PASTURE WASH/DENSE	0.220 0.180	6.90 2.80							
			32.00	0.208		0.248	2.070	9.70	4.98

Executed: 22:03:48 09-04-2003

# SANTA FE RANCH SUBDIVISION - FRUITA DEVELOPED RUNOFF - TOTAL SITE 9/1/03

\* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres

adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 2 years
'C' adjustment, k = 1
Adj. 'C' = Wtd.'C' x 1

Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd.	Adj. 'C'	I in/hr	Total acres	Peak Q (cfs)
DEVELOPED WASH/DENSE	0.330 0.180	6.90 2.80			= =			
			20.00	0.287	0.287	0.680	9.70	1.89

Executed: 22:03:48 09-04-2003

# SANTA FE RANCH SUBDIVISION - FRUITA DEVELOPED RUNOFF - TOTAL SITE 9/1/03

\* \* \* \* \* \* SUMMARY OF RATIONAL METHOD PEAK DISCHARGES \* \* \* \* \* \*

Q = adj \* C \* I \* A

Where: Q=cfs, C=Weighted Runoff Coefficient, I=in/hour, A=acres adj = 'C' adjustment factor for each return frequency

RETURN FREQUENCY = 100 years 'C' adjustment, k = 1.2414 Adj. 'C' = Wtd.'C' x 1.2414

Subarea Descr.	Runoff 'C'	Area acres	Tc (min)	Wtd. 'C'	Adj. 'C'	======================================	Total acres	Peak Q (cfs)
DEVELOPED WASH/DENSE	0.330 0.180	6.90 2.80						
			20.00	0.287	0.356	2.700	9.70	9.32

SECTION 5
HYDRAULICS

# SANTA FE RANCH - STORM OUTLET CHANNEL Worksheet for Trapezoidal Channel

Project Description	on
Project File	c:\haestad\fmw\santa fe.fm2
Worksheet	OUTLET CHANNEL
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Discharge

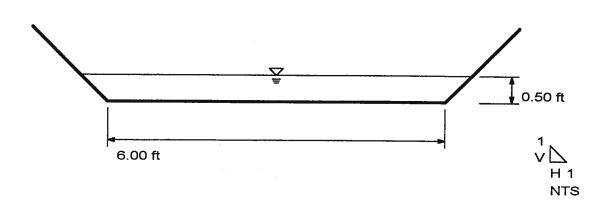
Input Data	
Mannings Coefficient	0.013
Channel Slope	0.005000 ft/ft
Depth	0.50 ft
Left Side Slope	1.000000 H : V
Right Side Slope	1.000000 H : V
Bottom Width	6.00 ft

Results		
Discharge	15.16	cfs
Flow Area	3.25	ft²
Wetted Perimeter	7.41	ft
Top Width	7.00	ft
Critical Depth	0.56	ft
Critical Slope	0.0033	34 ft/ft
Velocity	4.66	ft/s
Velocity Head	0.34	ft
Specific Energy	0.84	ft
Froude Number	1.21	
Flow is supercritical.		

### SANTA FE RANCH - STORM OUTLET PAN Cross Section for Trapezoidal Channel

Project Description	n
Project File	c:\haestad\fmw\santa fe.fm2
Worksheet	OUTLET CHANNEL
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Discharge

Section Data		
Mannings Coefficient	0.013	
Channel Slope	0.005000	ft/ft
Depth	0.50	ft
Left Side Slope	1.000000	H:V
Right Side Slope	1.000000	H:V
Bottom Width	6.00	ft
Discharge	15.16	cfs



## SANTA FE RANCH - STORM OUTLET PIPE Worksheet for Circular Channel

Project Descriptio	n
Project File	c:\haestad\fmw\santa fe.fm2
Worksheet	Storm Outlet
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Mannings Coefficient	0.013	
Channel Slope	0.0500	00 ft/ft
Depth	1.25	ft
Diameter	15.00	in

Results		
Discharge	14.44	cfs
Flow Area	1.23	ft²
Wetted Perimeter	3.93	ft
Top Width	0.33e-7	ft
Critical Depth	1.23	ft
Percent Full	100.00	
Critical Slope	0.04559	4 ft/ft
Velocity	11.77	ft/s
Velocity Head	2.15	ft
Specific Energy	3.40	ft
Froude Number	0.34e-3	
Maximum Discharge	15.54	cfs
Full Flow Capacity	14.44	cfs
Full Flow Slope	0.050000	) ft/ft
Flow is subcritical.		

# Table Rating Table for Circular Channel

Project Description	n
Project File	c:\haestad\fmw\santa fe.fm2
Worksheet	Storm Outlet
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Discharge

Constant Data	
Mannings Coefficient	0.013
Depth	1.25 ft
Diameter	15.00 in

Input Data			
	Minimum	Maximum	Increment
Channel Slope	0.005000	0.050000	0.005000 ft/ft

Rating Table	
Channel	
Slope	Discharge
(ft/ft)	(cfs)
*	
0.005000	4.57
0.010000	6.46
0.015000	7.91
0.020000	9.14
0.025000	10.21
0.030000	11.19
0.035000	12.08
0.040000	12.92
0.045000	13.70
0.050000	14.44

